

Mitigating Moisture-Related Road Problems with Wicking Geotextile

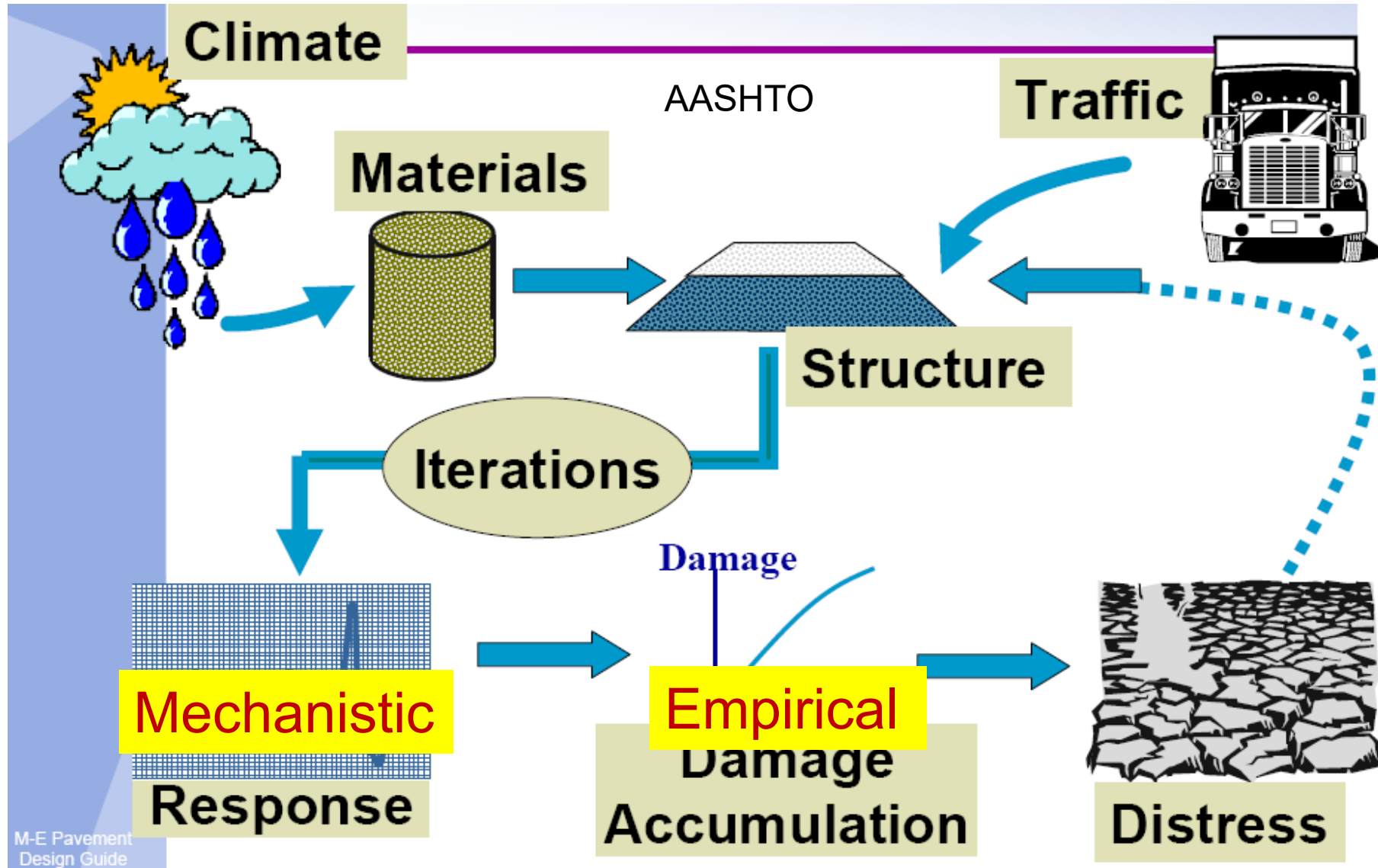
Jie Han, Ph.D., PE, F.ASCE

**Roy A. Roberts Distinguished Professor
The University of Kansas**

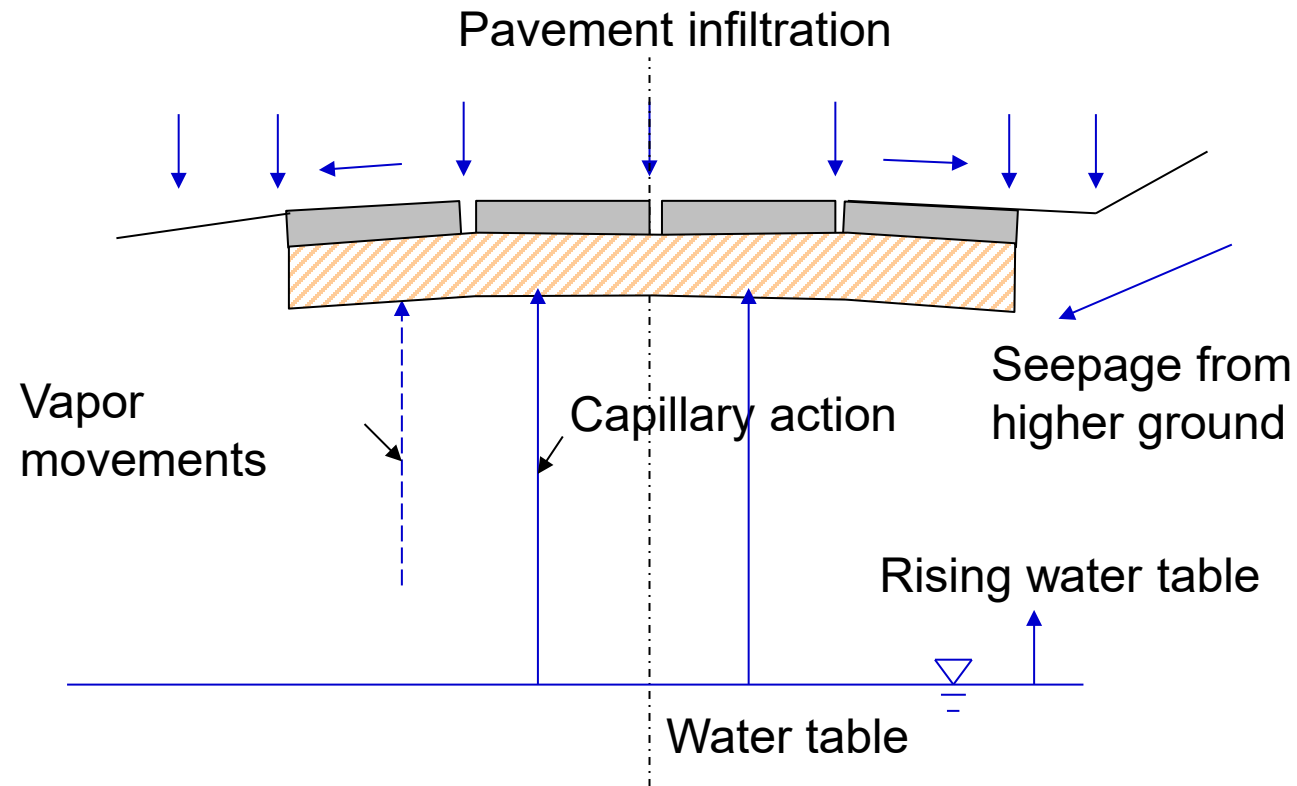
Outline of Presentation

- **Introduction**
- **Mechanisms and Benefits**
- **Laboratory Tests and Results**
- **Case Studies**
- **Concluding Remarks**

Mechanistic-Empirical (M-E) Pavement Design



Source and Effect of Water



- Reduction of soil strength and stiffness
- Erosion of concrete pavement
- Soil expansion
- Migration of fines
- Freeze-thaw

Moisture-related Pavement Distresses



Fines migration

Lawrence, Kansas, USA



Freeze-thaw cycles

Montreal, Canada, 9/15/2024

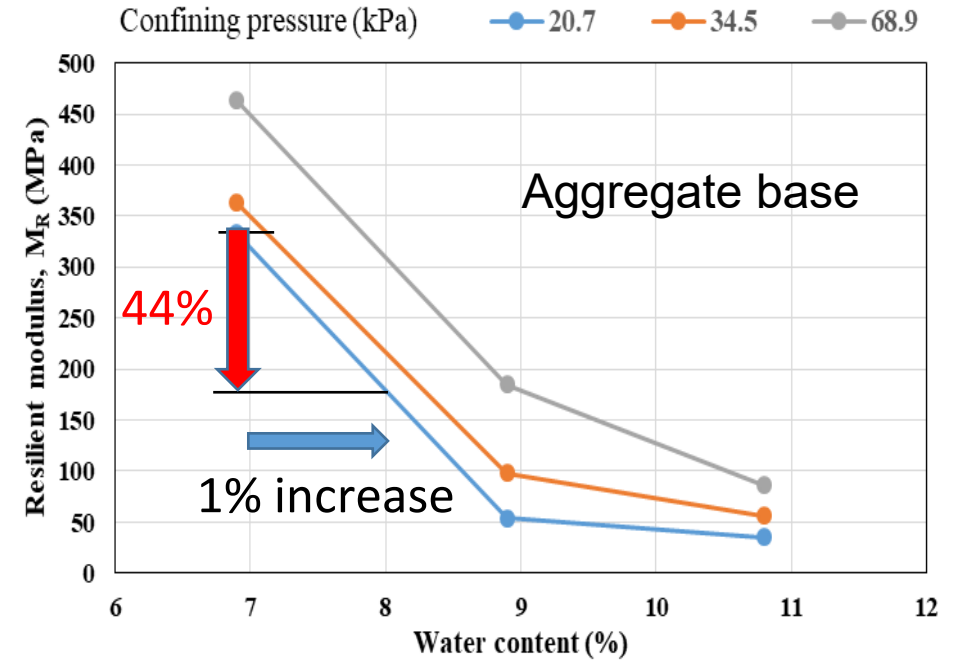
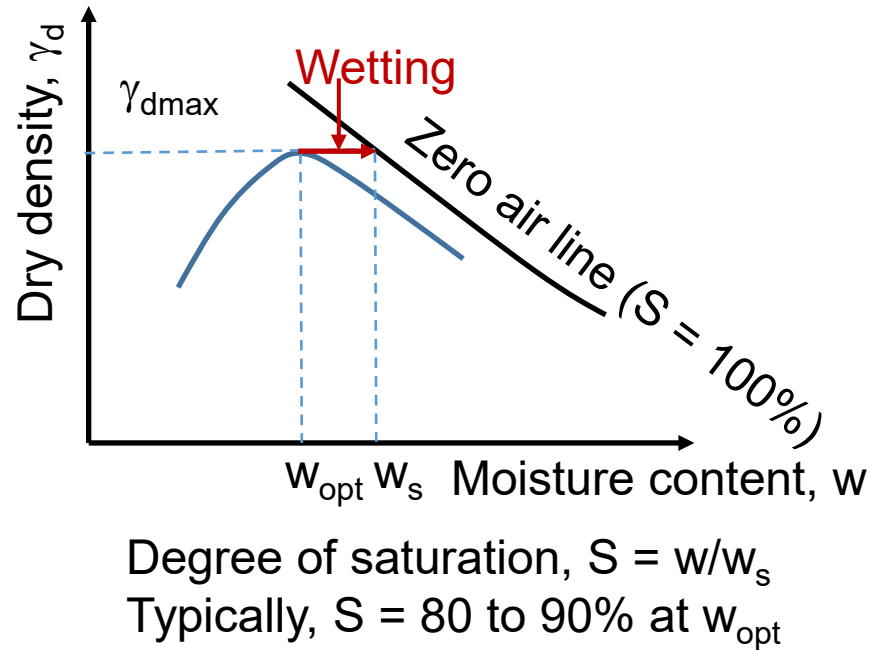
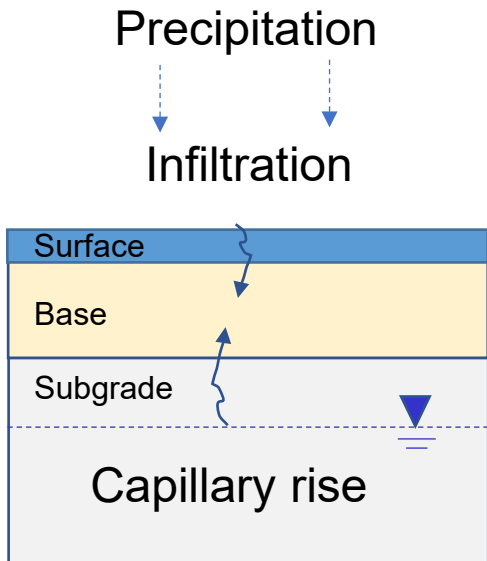
Moisture-related Pavement Distresses



Credit: City of Edmonton, Canada

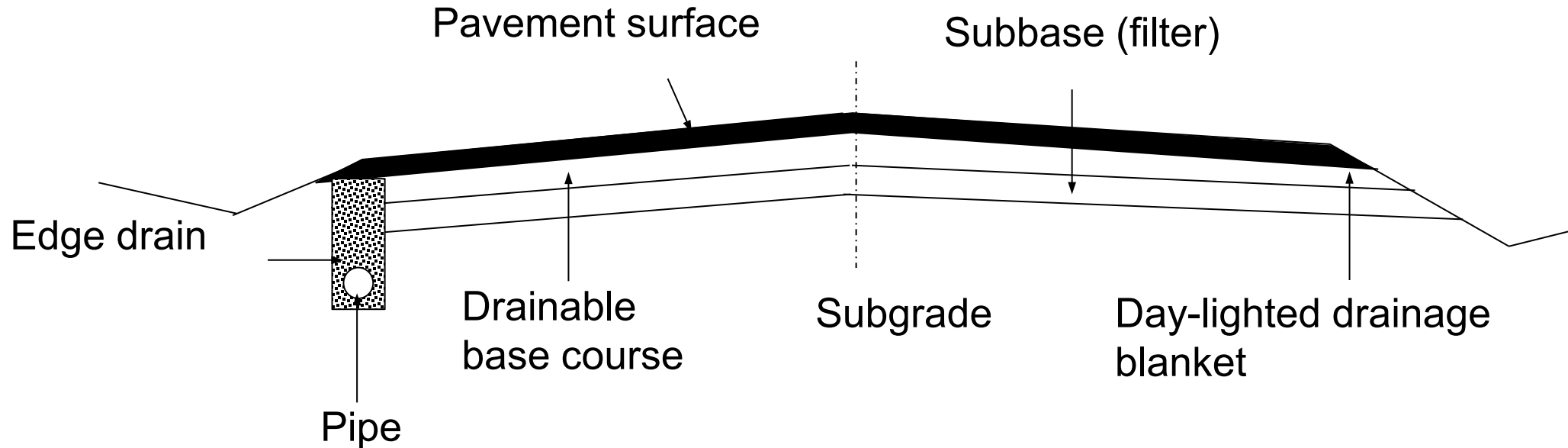
Failed after one freeze-thaw cycle due to high groundwater table

Behavior of Compacted Soil



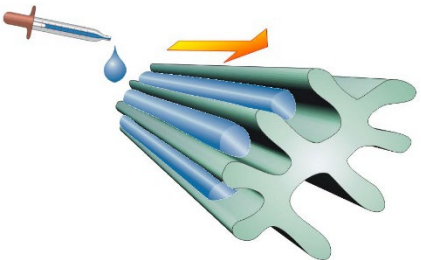
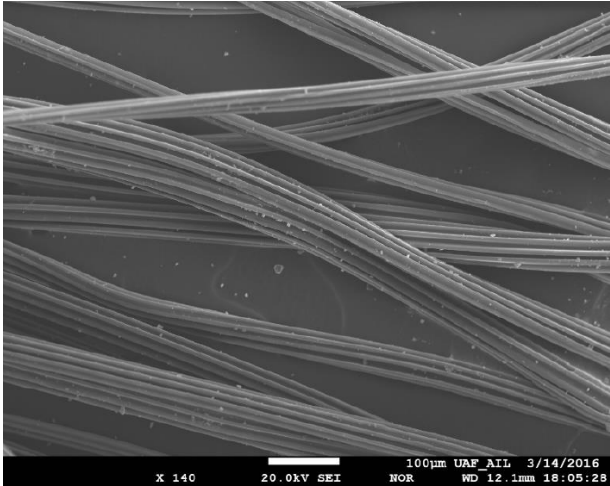
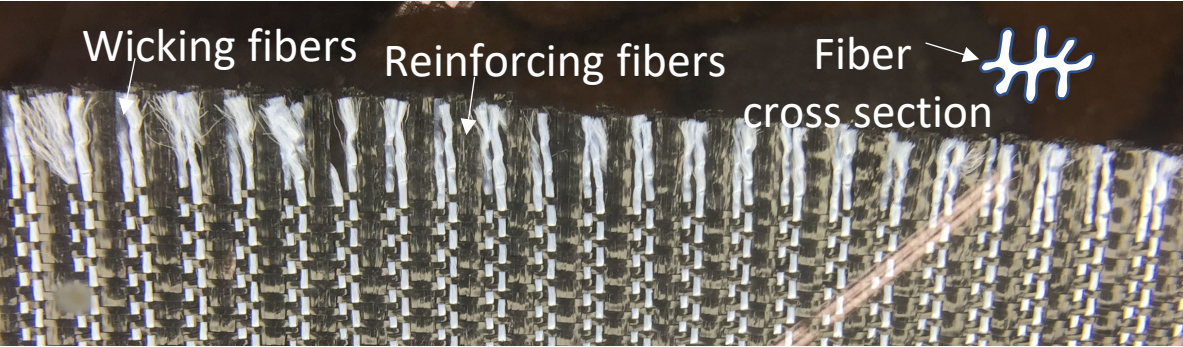
Plotted from Lin et al. (2019)

Road Drainage and Problems

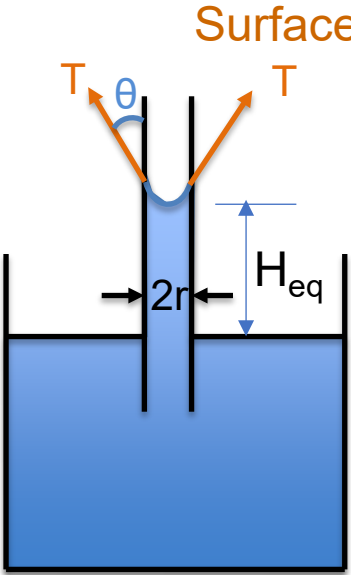


1. Conventional approach: use drainage materials (aggregate, sand layers, or geotextile), only reducing moisture content to a field capacity condition
2. Road condition: often unsaturated and subjected to capillary rise

Wicking Geotextile



Deep-grooved fiber
Groove diameter: 30-50 μm
Groove spacing: 5-12 μm



Capillary rise height

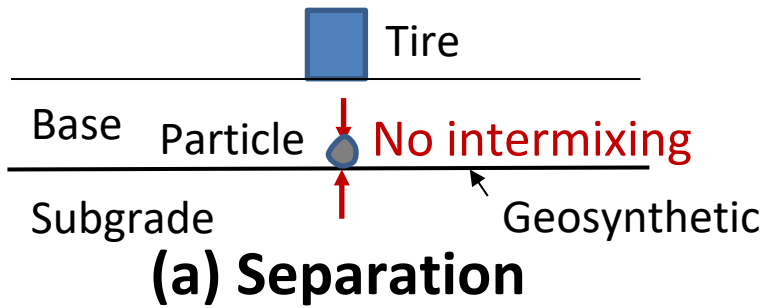
Suction

$$H_{eq} = \frac{2T \cos \theta}{r}$$

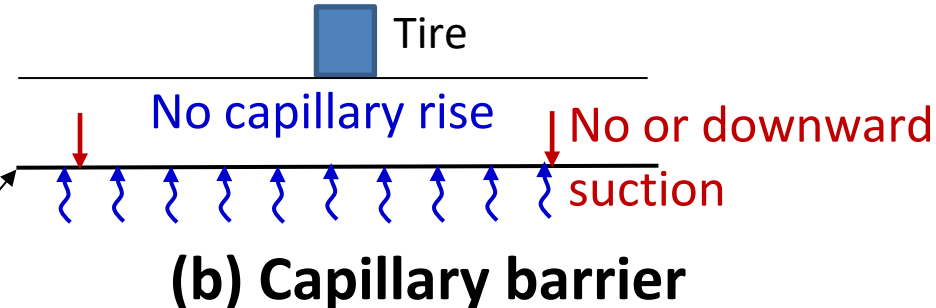
$$u_f = H_{eq} \gamma = \frac{2T \cos \theta}{r}$$

T = liquid surface tension; θ = contact angle;
γ = unit weight of liquid; r = capillary radius

Mechanisms & Benefits of Geosynthetics in Roads

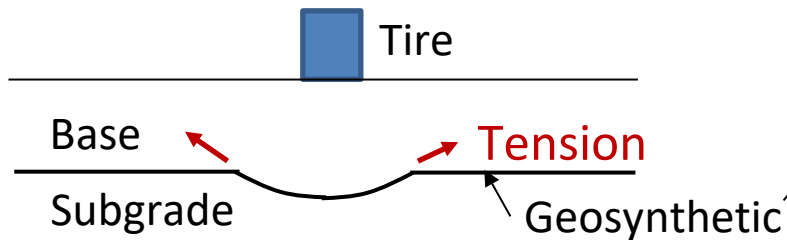


(a) Separation

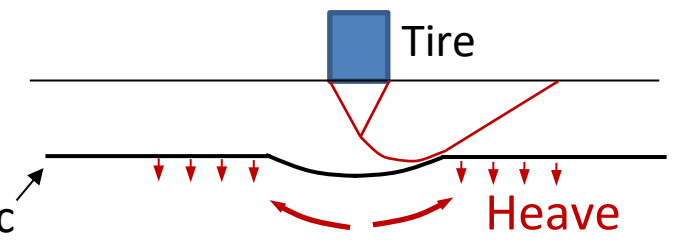


(b) Capillary barrier

Maintain strength & modulus of base course

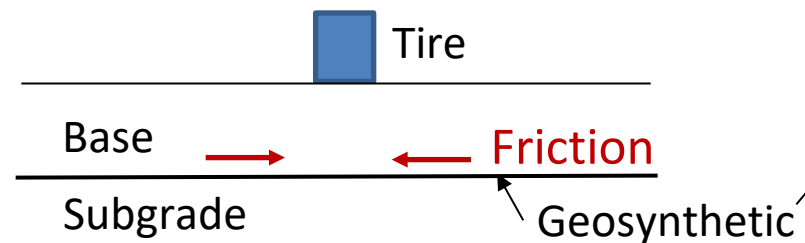


(c) Tensioned membrane

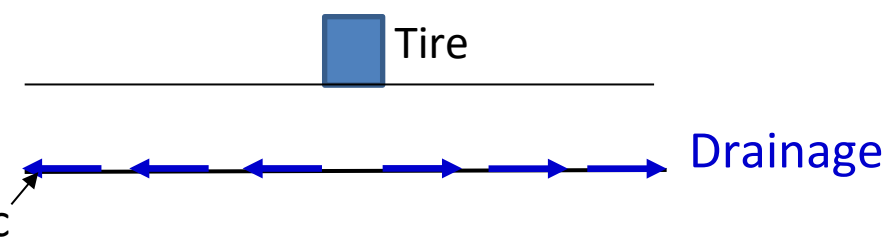


(d) Vertical restraint

Increase strength of subgrade & base course



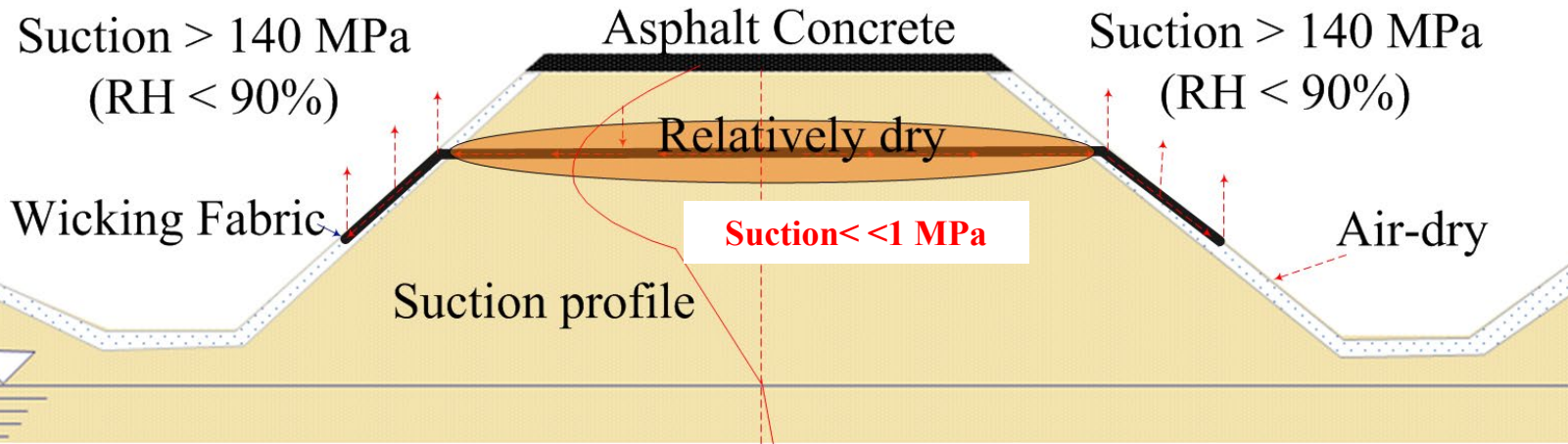
(e) Lateral restraint



(f) Lateral drainage

Increase strength & modulus of base course

Wicking Geotextile to Remove Water in Pavement Structure



Courtesy of J. Lostumbo

Suction in air
(Fredlund and Rahardjo 1993)

$$u_a = -\frac{RT\rho_w}{M_w} \ln(RH)$$

R = universal gas constant (8.31432 J mol⁻¹ K⁻¹), T = absolute temperature, ρ_w = density of water as a function of temperature, M_w = molecular mass of water vapor, and RH = relative humidity.

$$u_a > u_f > u_s$$

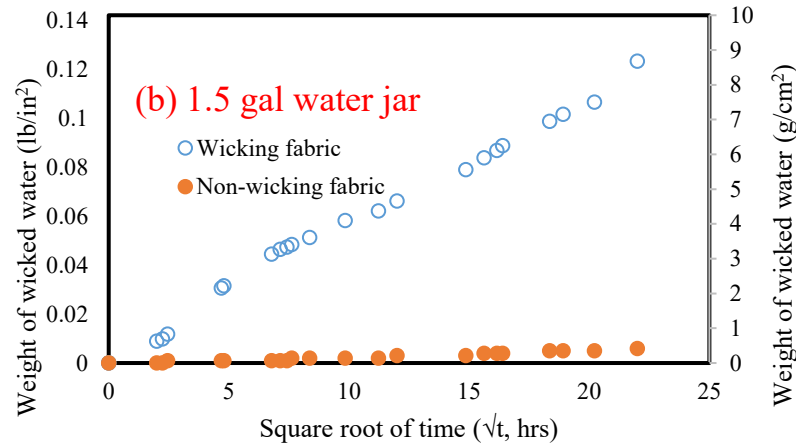
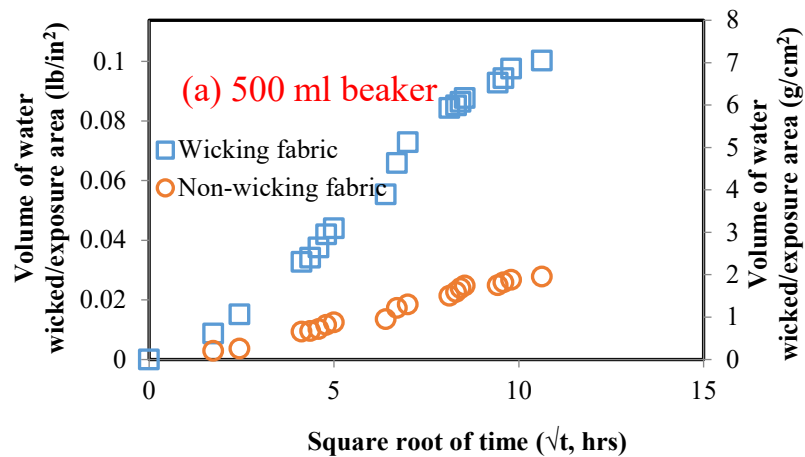
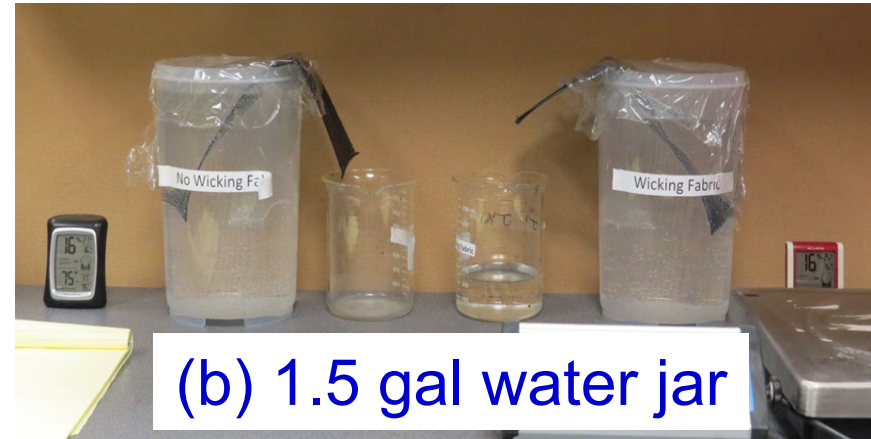
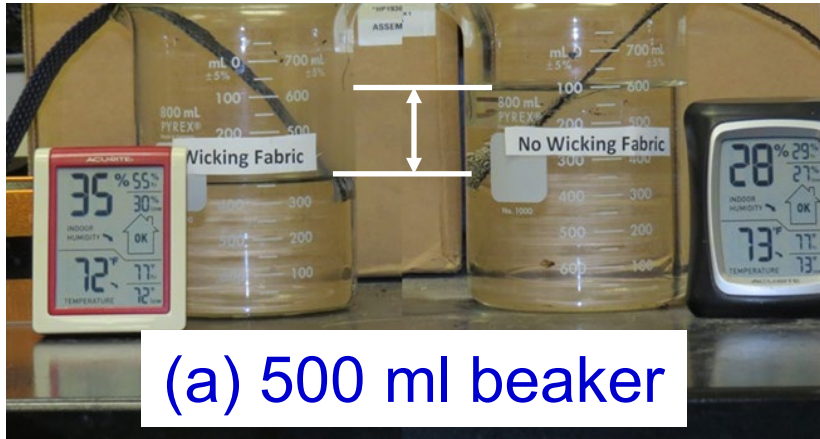
Air Fibers Soil

Zhang et al. (2014)

Wicking vs. Non-wicking Geotextile

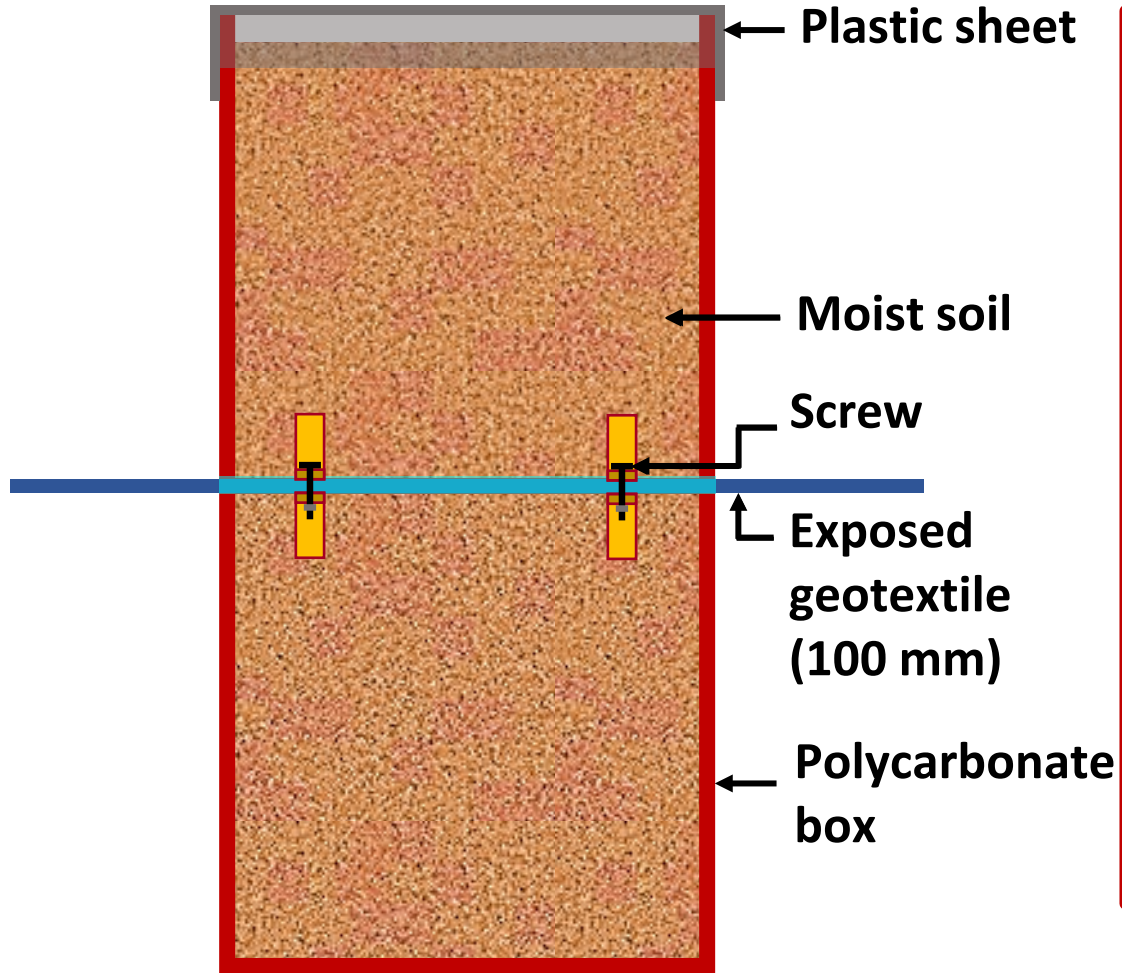
Top open

Top covered



Almost no water was wicked out by the non-wicking geotextile !!

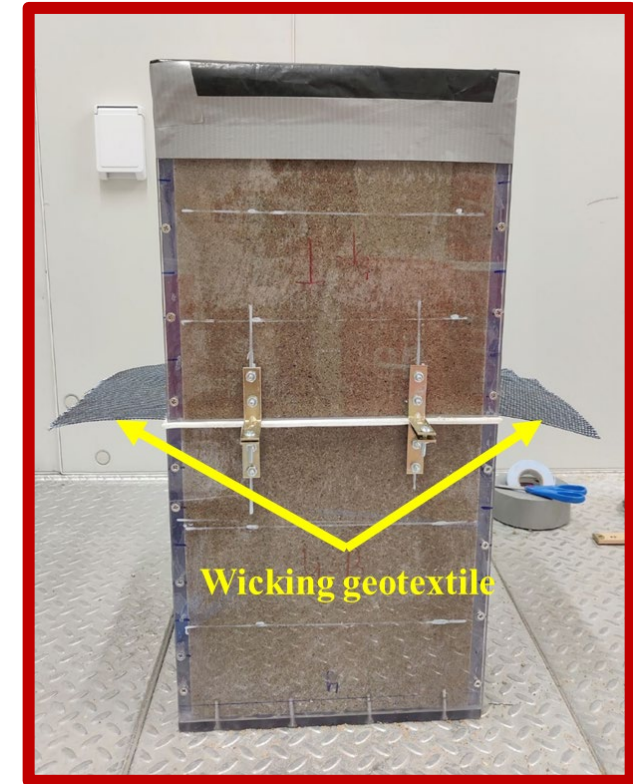
Moisture Reduction Tests



300 x 300 x 600 mm high



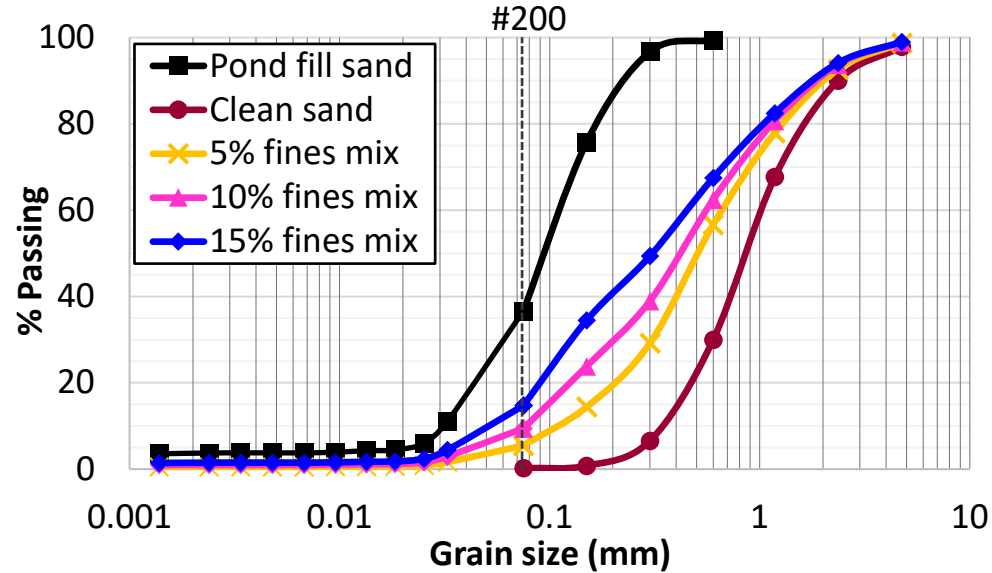
Controlled Room
T ~10°C, RH ~50%



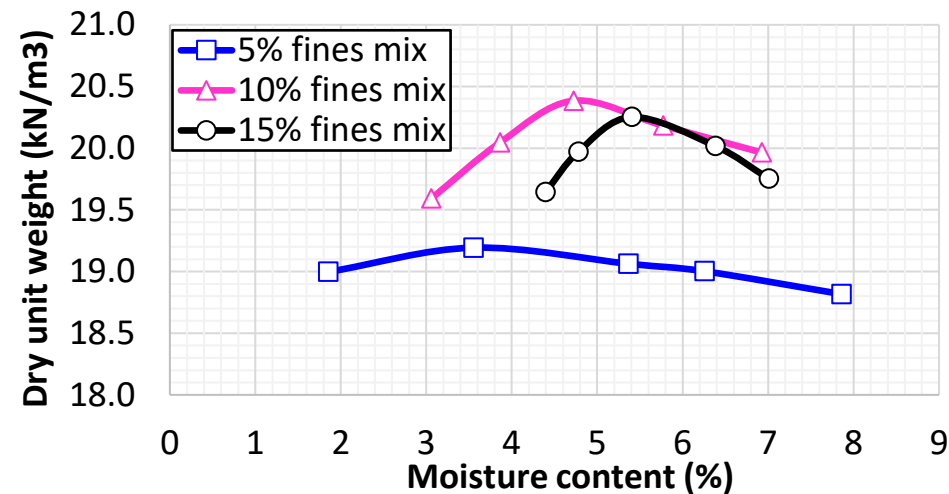
Fines Effect



Pond fill sand collected



Particle size distribution



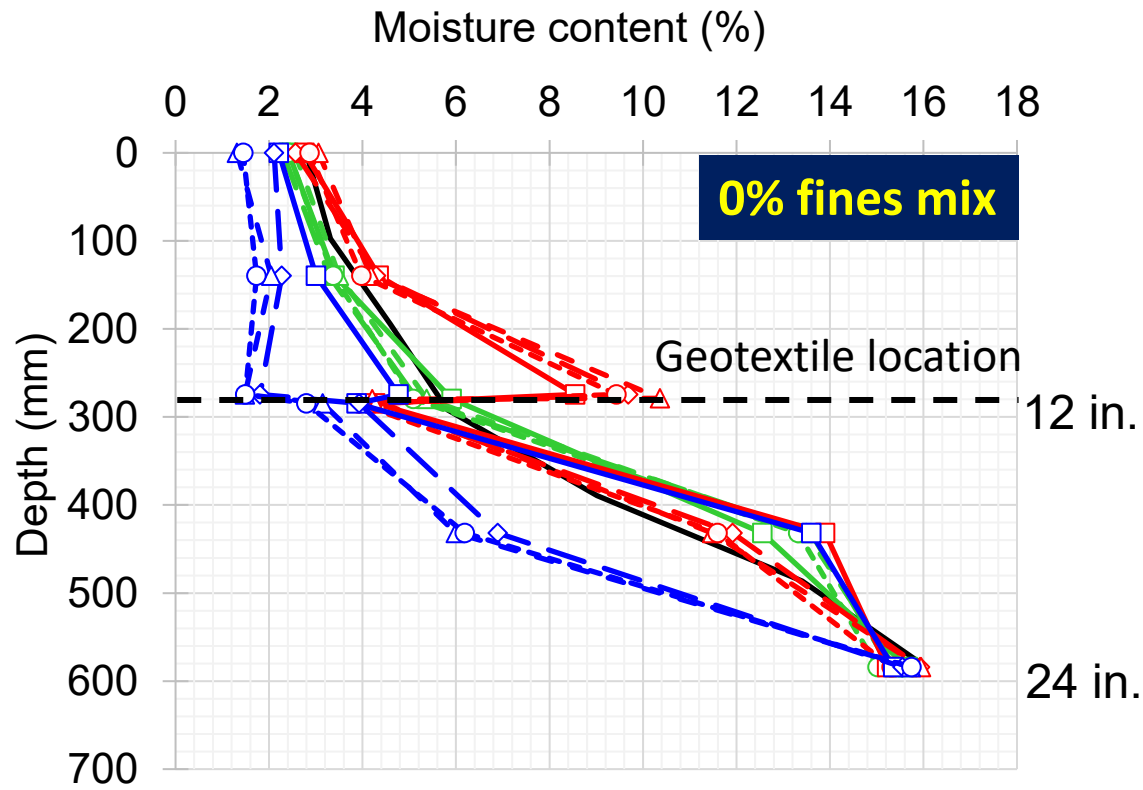
Standard Proctor compaction

Clean sand (0% fines):

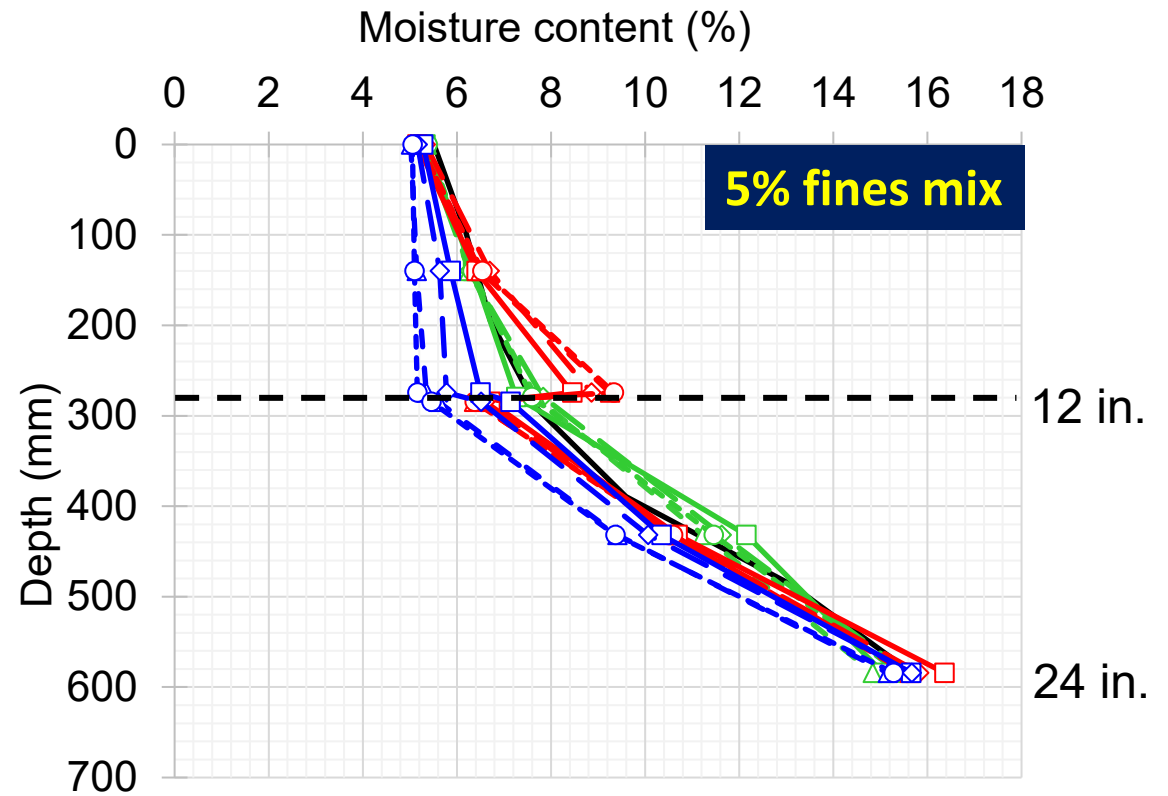
$$\gamma_{d,max} \text{ (kN/m}^3\text{)} = 18.85$$

$$\gamma_{d,min} \text{ (kN/m}^3\text{)} = 16.02$$

Moisture Reduction Test Results

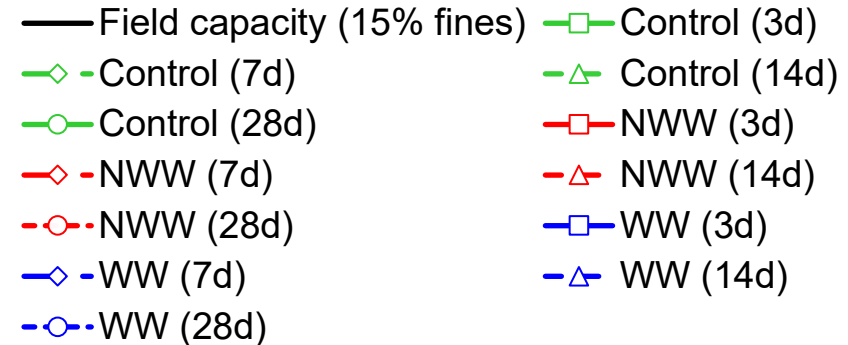
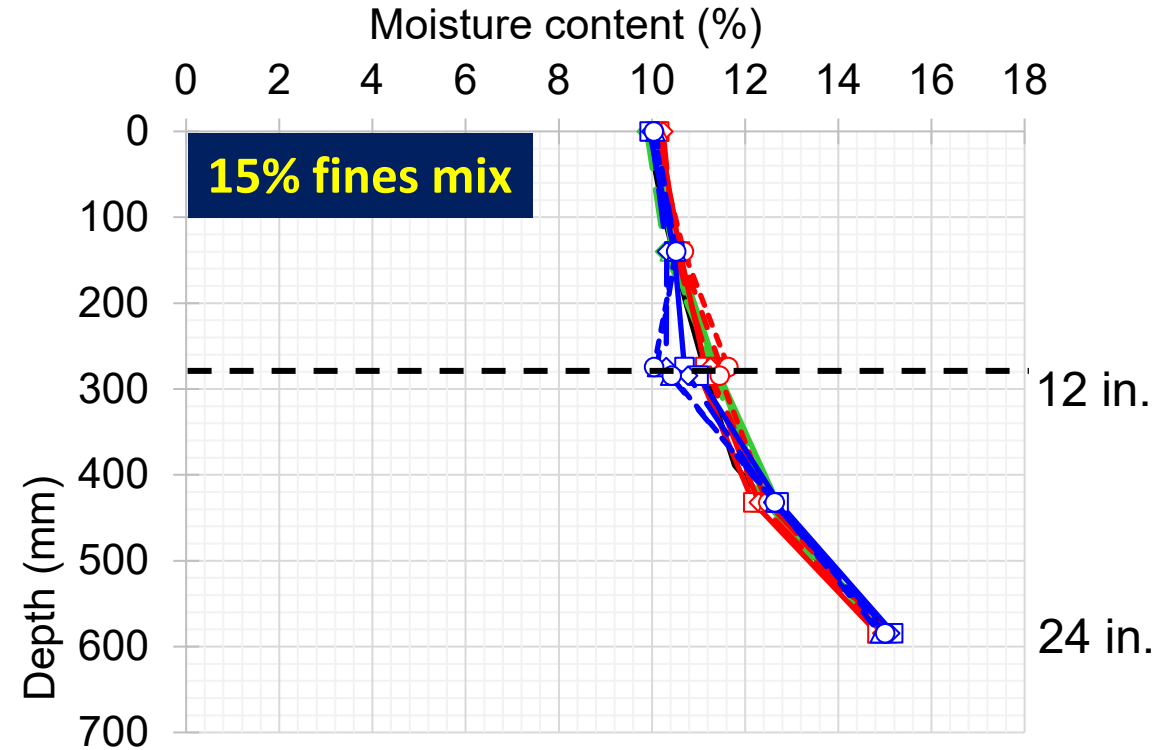
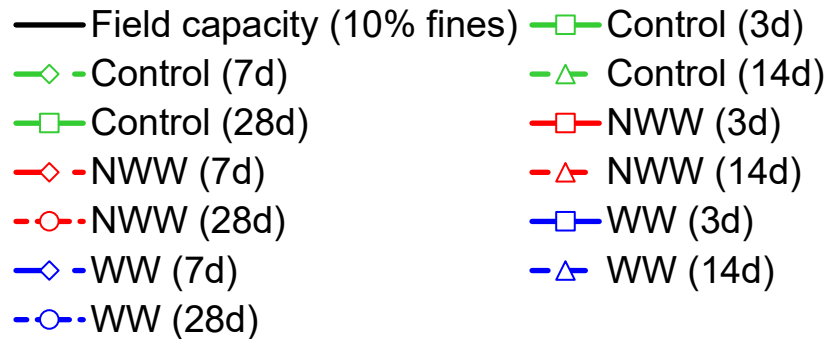
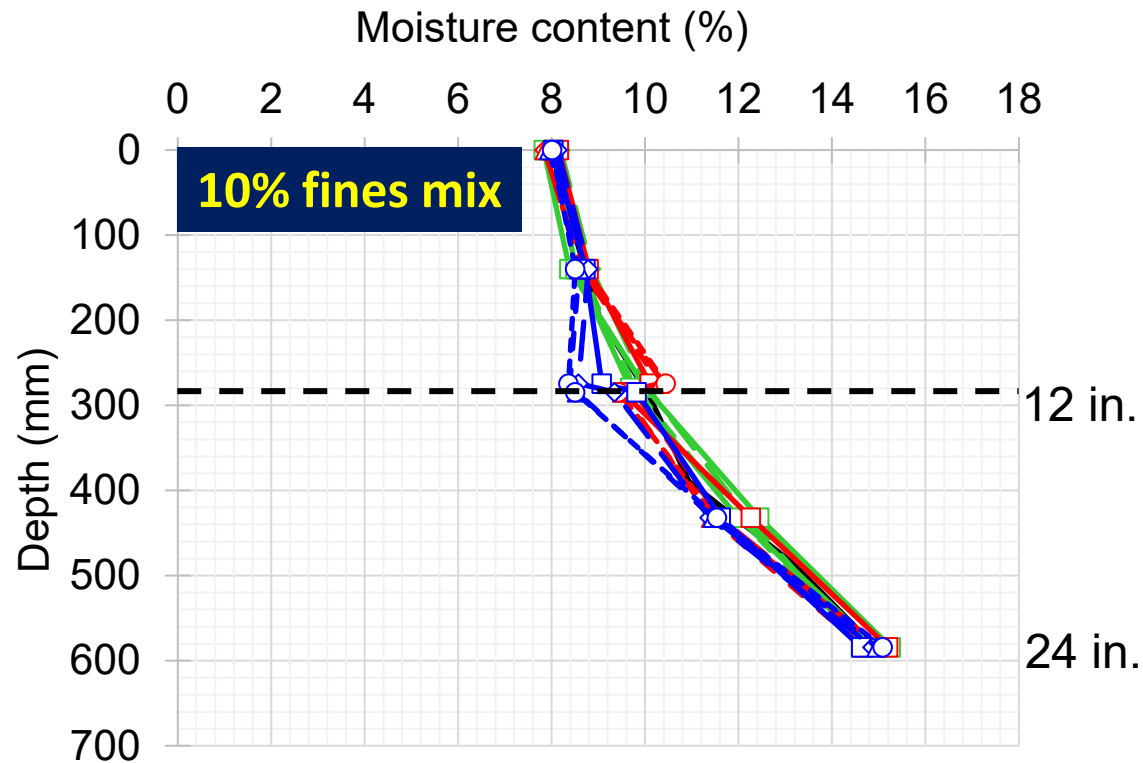


- Field capacity (0% fines)
- ◇— Control (3d)
- ◇— Control (7d)
- ◇— Control (14d)
- ◇— Control (28d)
- ◇— NWW (3d)
- ◇— NWW (7d)
- ◇— NWW (14d)
- ◇— NWW (28d)
- ◇— WW (3d)
- ◇— WW (7d)
- ◇— WW (14d)
- ◇— WW (28d)

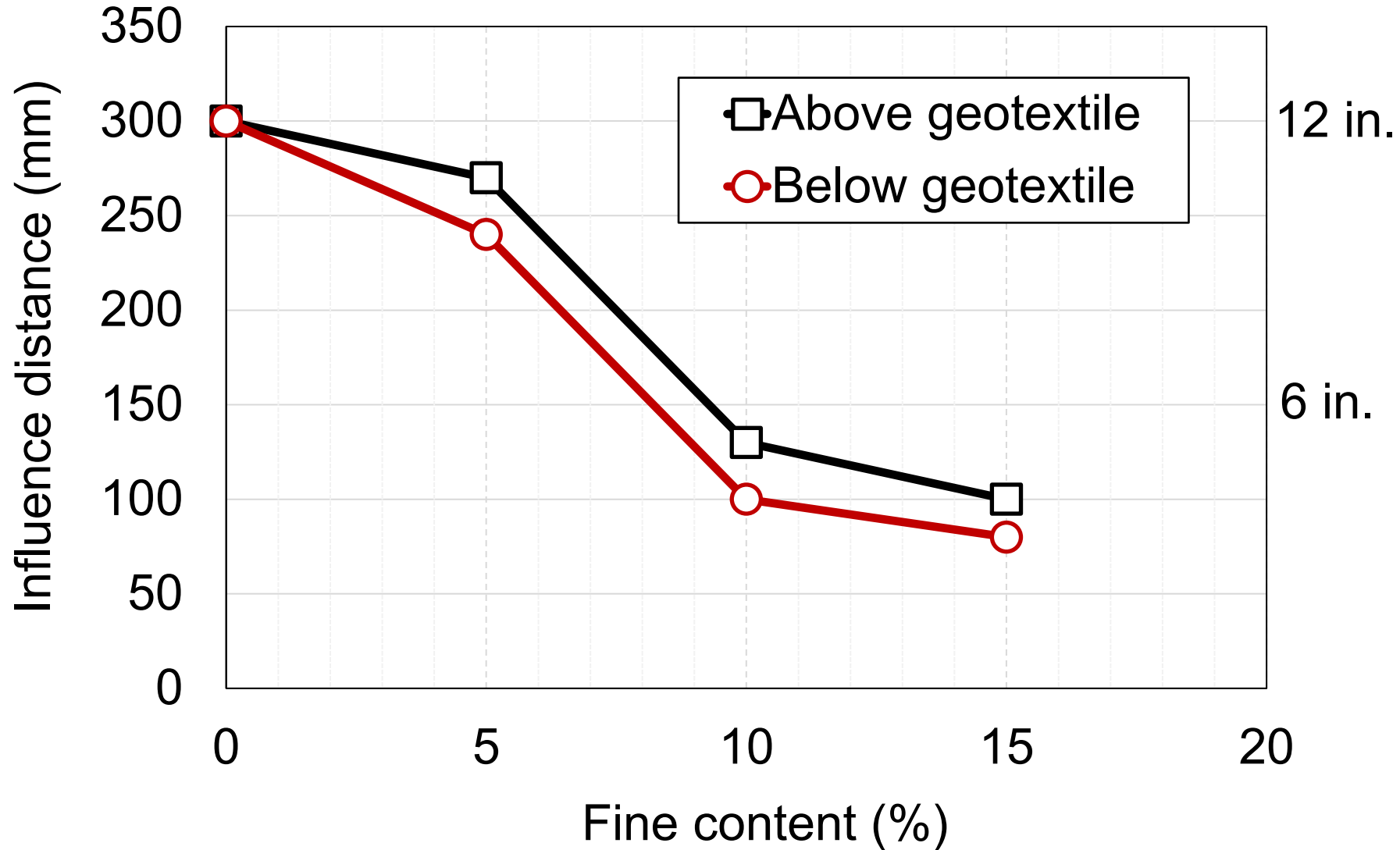


- Field capacity (5% fines)
- ◇— Control (3d)
- ◇— Control (7d)
- ◇— Control (14d)
- ◇— Control (28d)
- ◇— NWW (3d)
- ◇— NWW (7d)
- ◇— NWW (14d)
- ◇— NWW (28d)
- ◇— WW (3d)
- ◇— WW (7d)
- ◇— WW (14d)
- ◇— WW (28d)

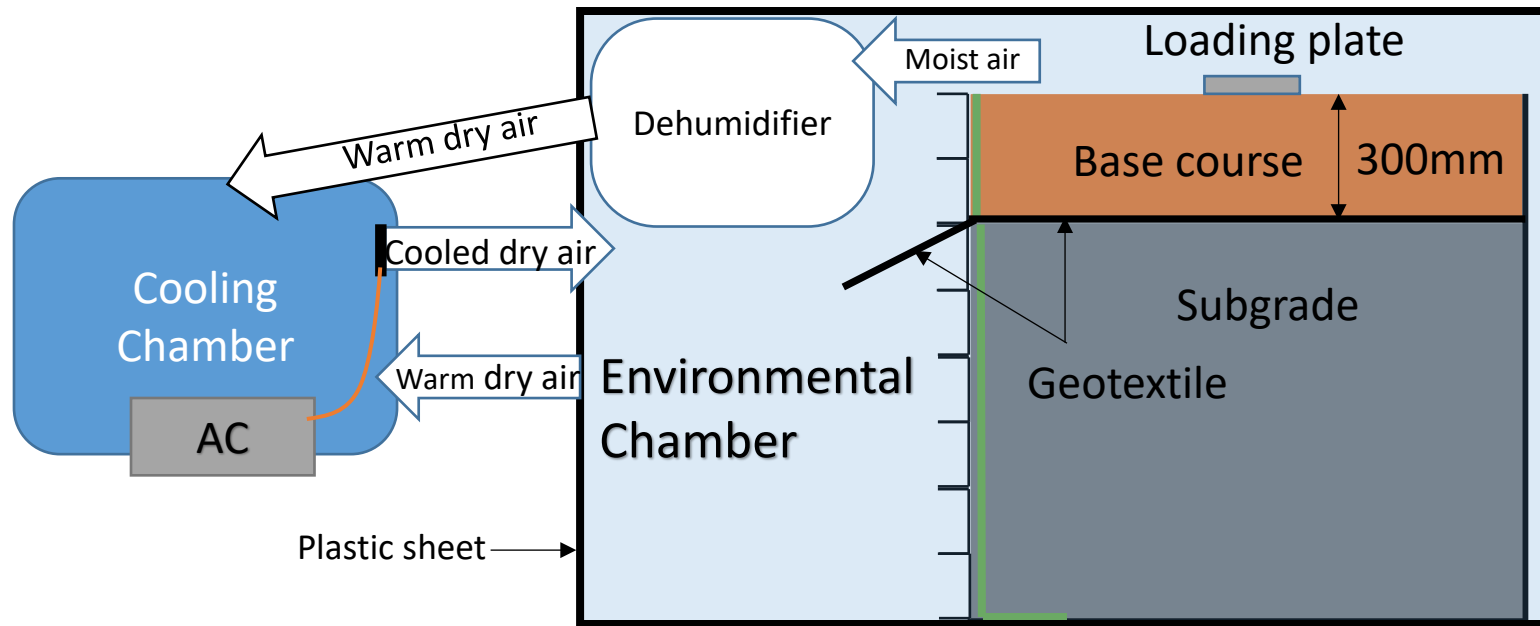
Moisture Reduction Test Results



Influence Distance of Wicking Geotextile



Large Box Tests



Test No.	Subgrade CBR	Geosynthetic
1	3.3%	N/A
2	2.9%	Non-wicking woven geotextile
3	3.1%	Wicking geotextile
4	4.7%	N/A
5	4.8%	Non-wicking woven geotextile
6	5.0%	Wicking geotextile



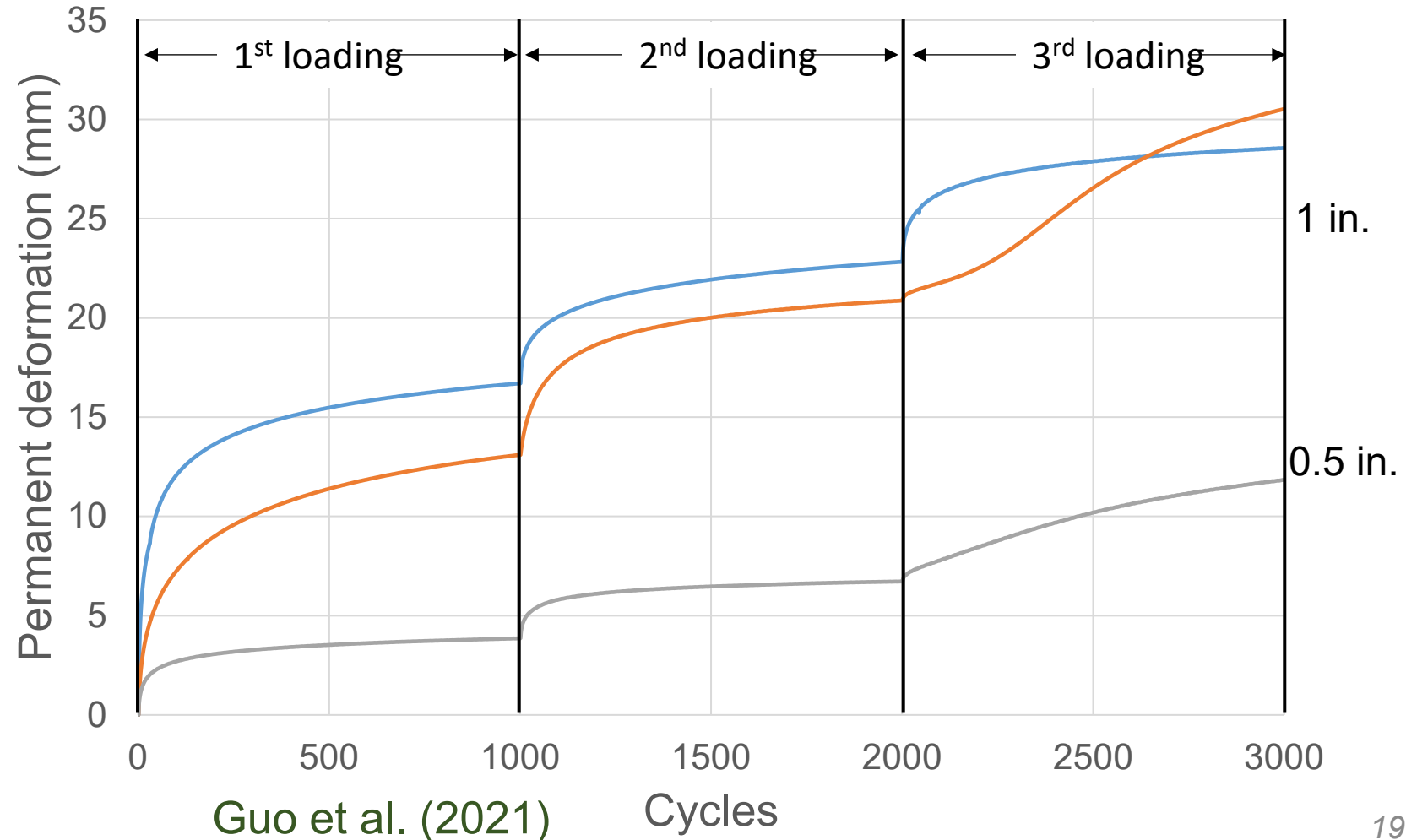
Guo, J., Han, J., Zhang, X., and Li, Z. (2021). "Experimental evaluation of wicking geotextile-stabilized aggregate bases over subgrade under rainfall simulation and cyclic loading." *Geotextiles and Geomembranes*, 49, 1550-1564.

Test Procedure and Results

1000 cycles of plate loading test at $p = 140 \text{ kPa}$ (20 psi)

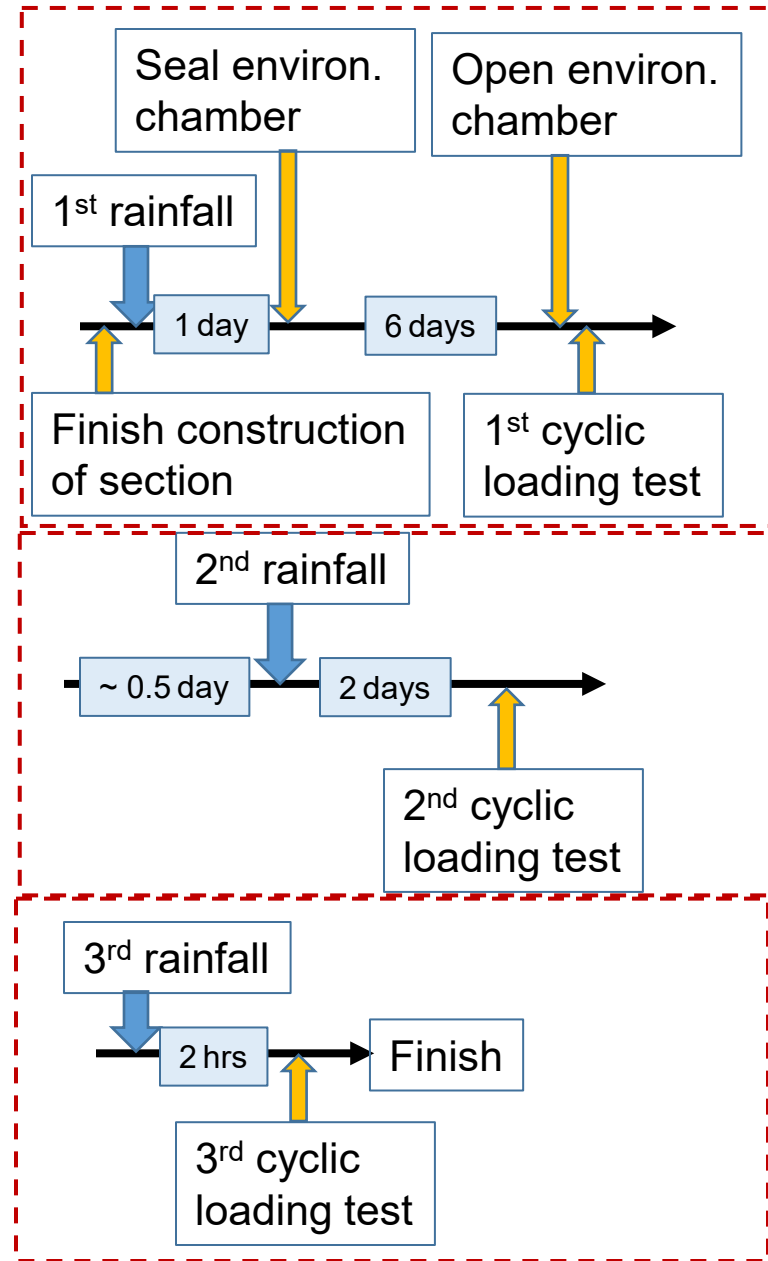
Stage 1

— 3% Control — 3% Non-wicking — 3% Wicking



2

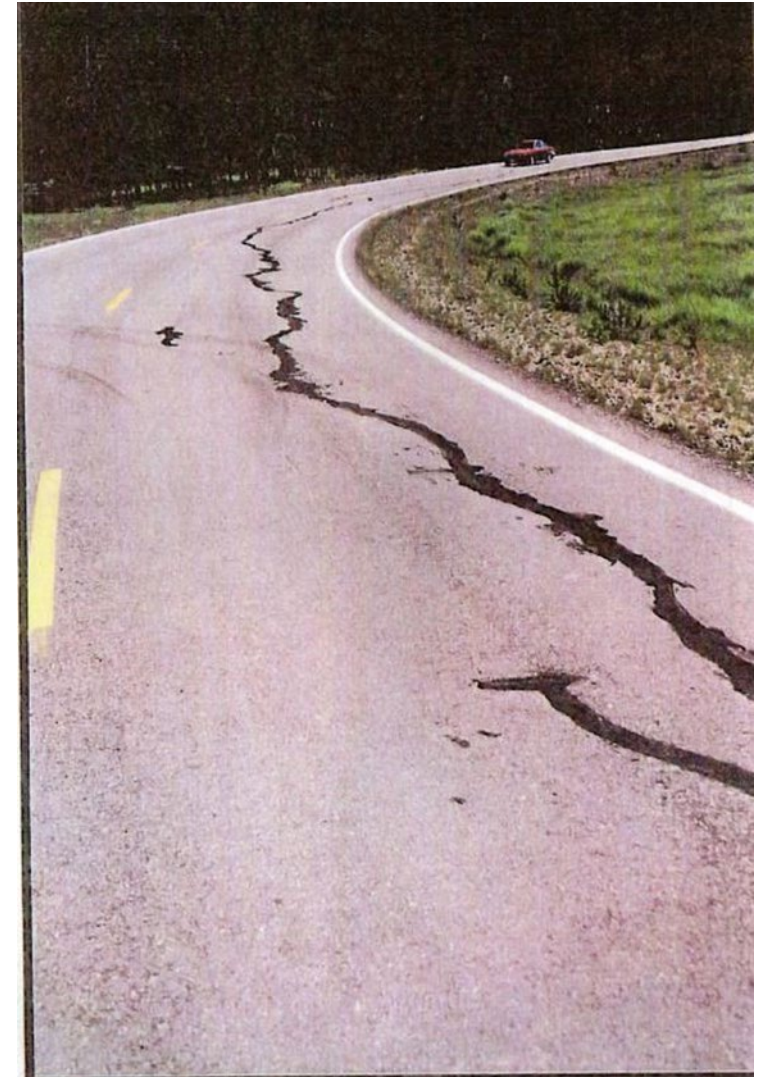
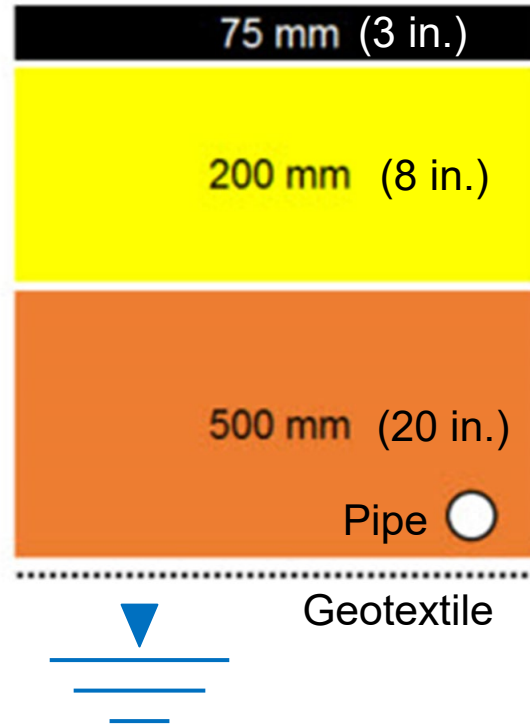
3



Frost Heave Prevention



Previous treatment



Courtesy of
J. Lostumbo

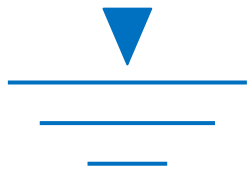
New Treatment with Wicking Geotextile

100 mm (4 in)

200 mm (8 in)
Reinforcement

250 mm (10 in)

Wicking Geotextile



Courtesy of
J. Lostumbo



Mitigating High Groundwater Table and Freeze-thaw Problems for Concrete Pavement



US169 in Iola, Kansas , USA

Pavement Condition before Reconstruction

Most frequent level of faulting

Fault Score per segment

Avg. no. of distressed joints per location

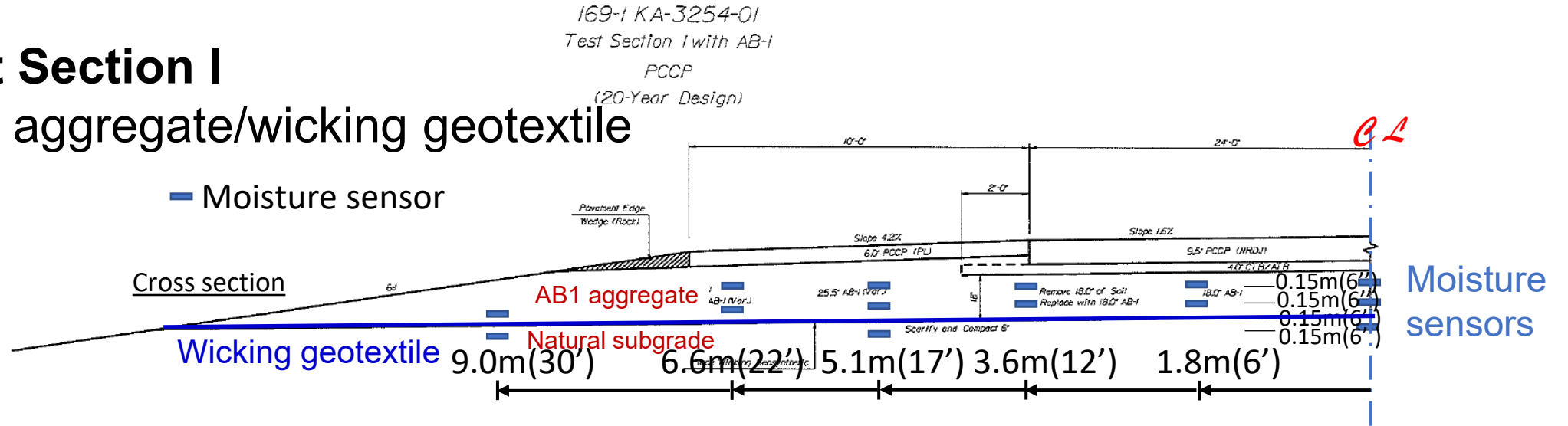
YEAR	LANE	RIDE			RIGID DISTRESS									
		IRI in/mi	Mays in/mi	PL	F	FS	J0	J1	J2	J3	J4	F1	F2	F3
2014	0	55	39	1	0.6	6.3	0.5	-	-	-	-	6.1	-	-
2015	0	68	50	1	-	-	-	-	-	-	-	-	-	-
2016	0	82	61	1	1.0	24.6	0.6	-	-	-	-	21.6	1.3	0.1
2017	0	88	68	1	1.3	34.1	1.8	0.3	0.1	-	-	26.6	3.0	0.4
2018	0	119	9	2	1.6	46.9	-	-	0.1	-	1.1	35.4	4.3	0.8

International Performance Roughness Level Index

Instrumented Test Sections with Moisture Sensors

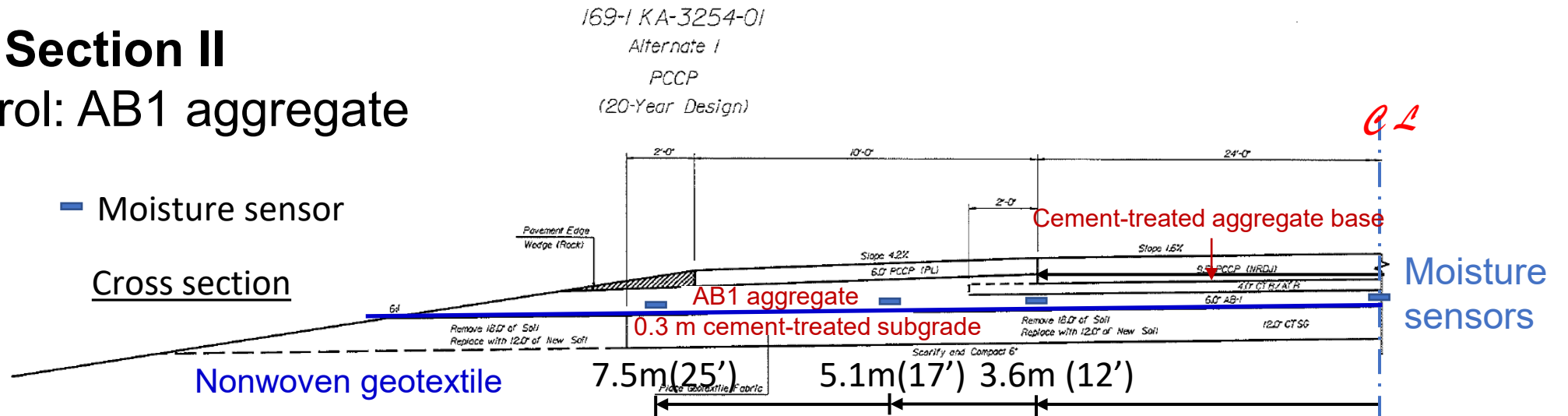
Test Section I

AB1 aggregate/wicking geotextile



Test Section II

Control: AB1 aggregate

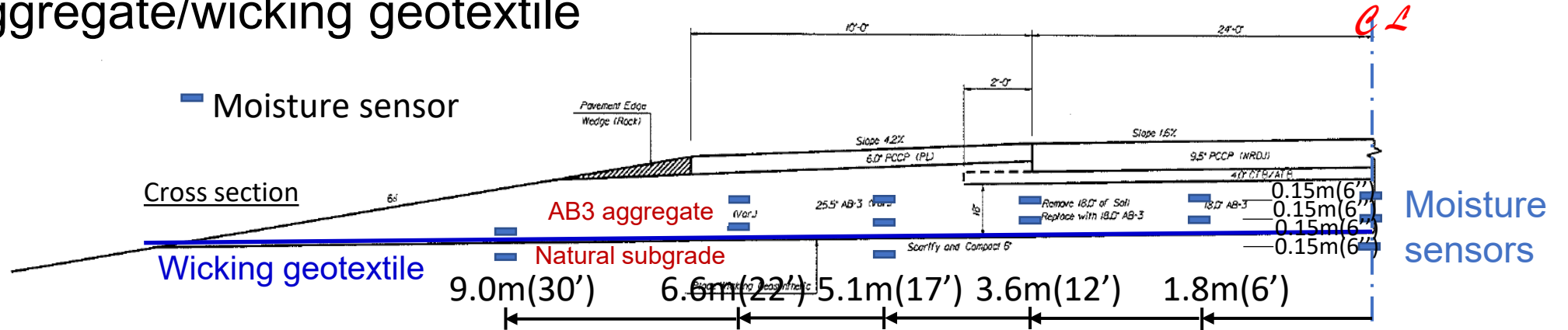


Instrumented Test Sections with Moisture Sensors

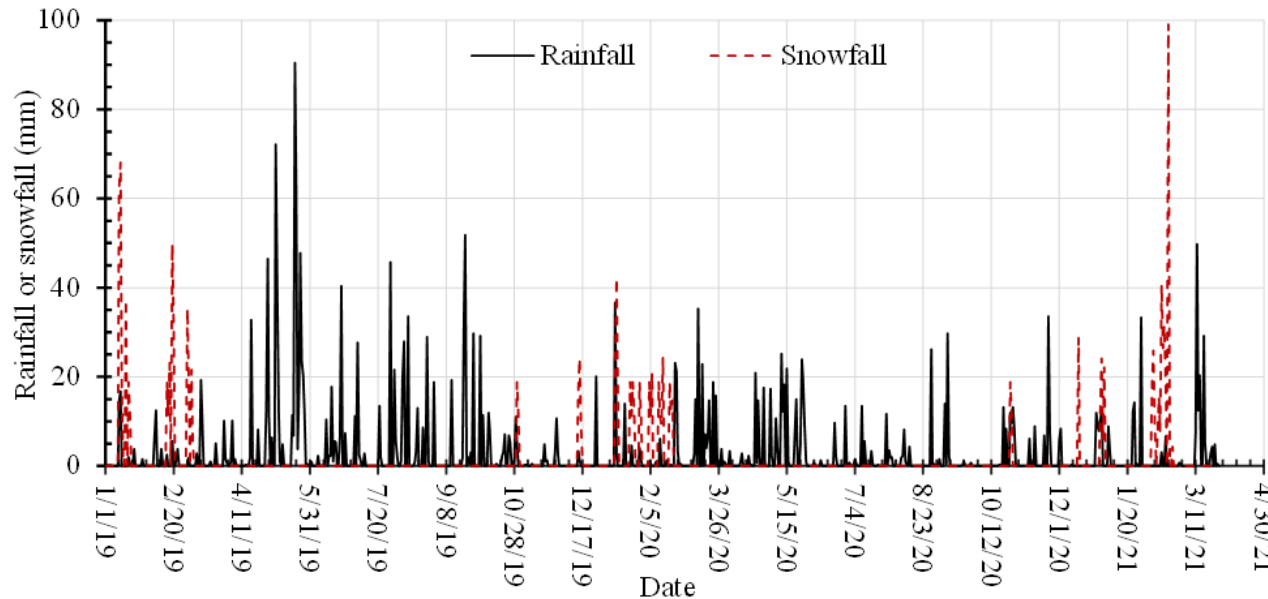
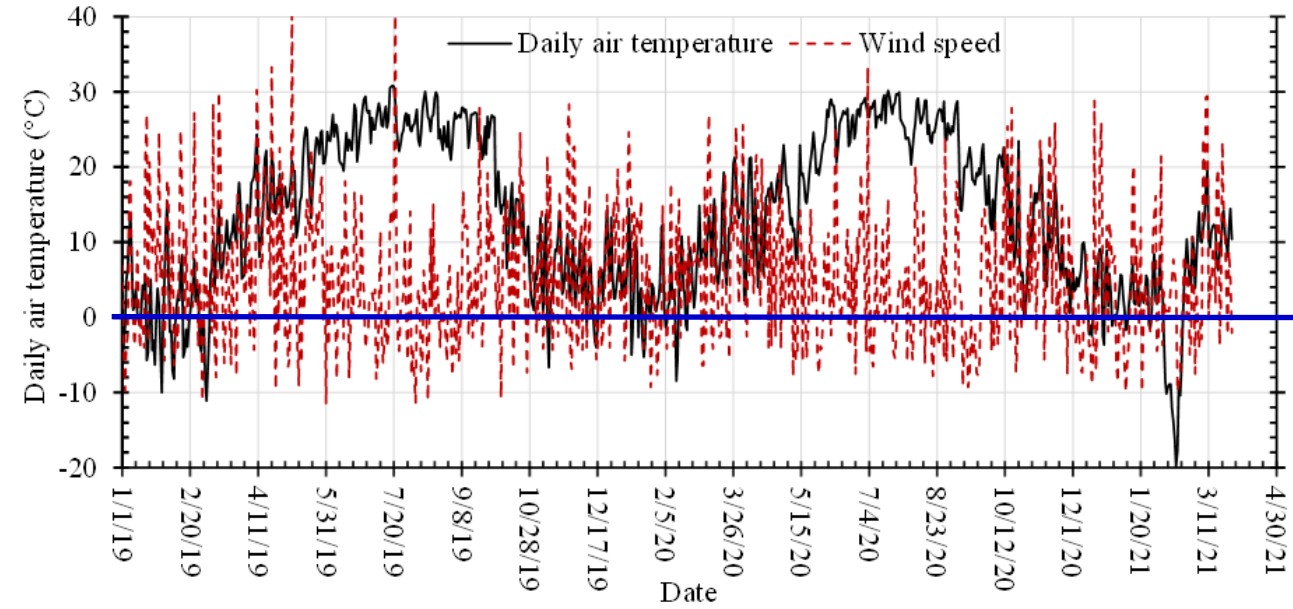
169-1 KA-3254-01
Test Section I with AB-3
PCCP
(20-Year Design)

Test Section III

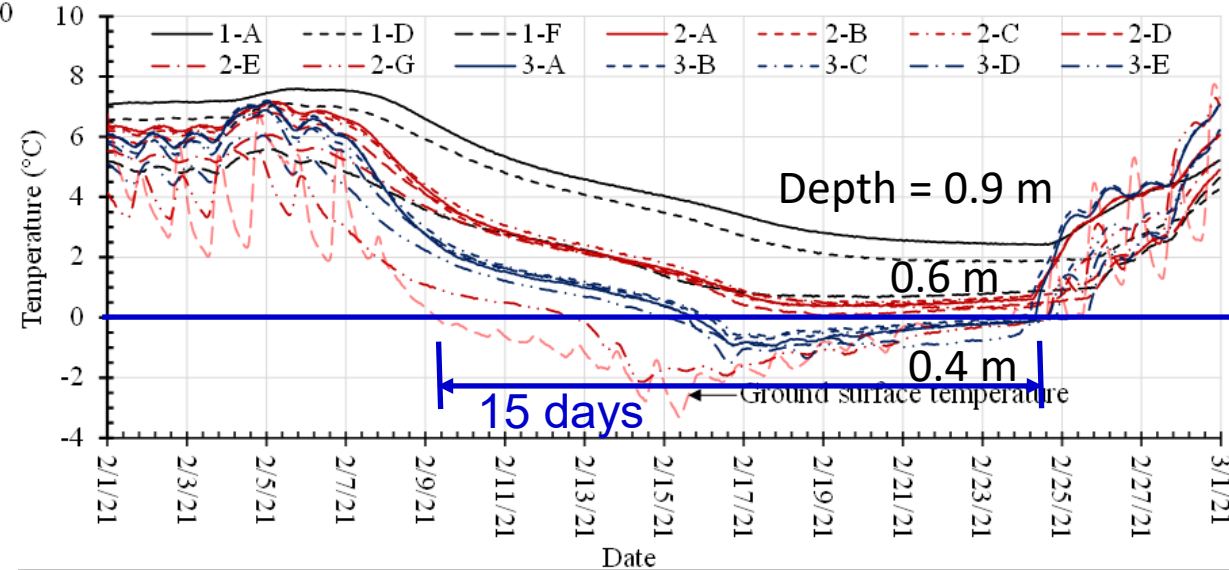
AB3 aggregate/wicking geotextile



Climatic Condition



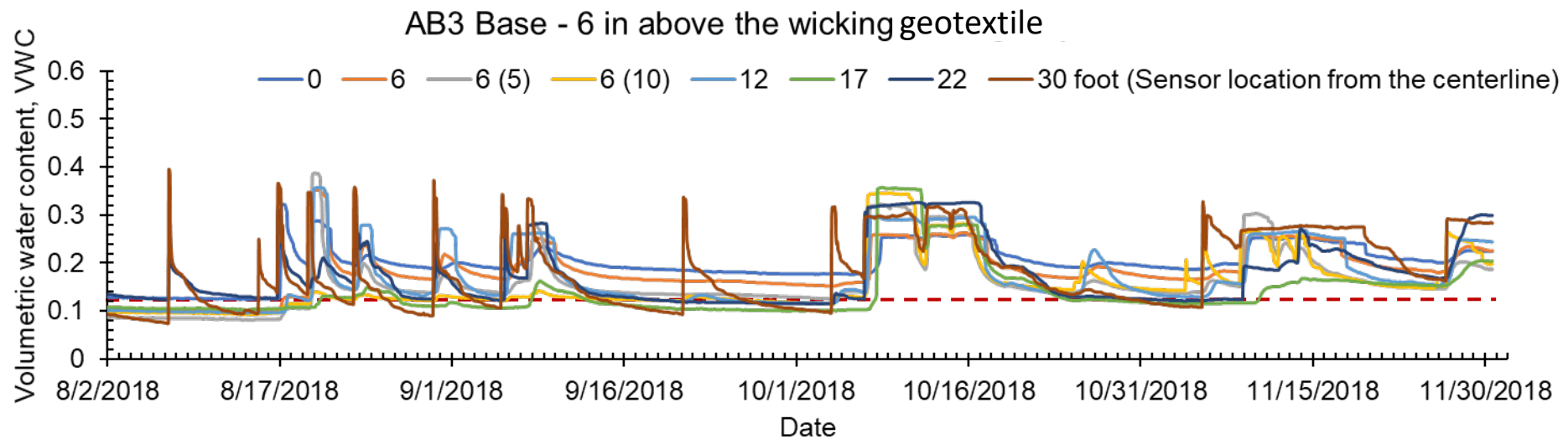
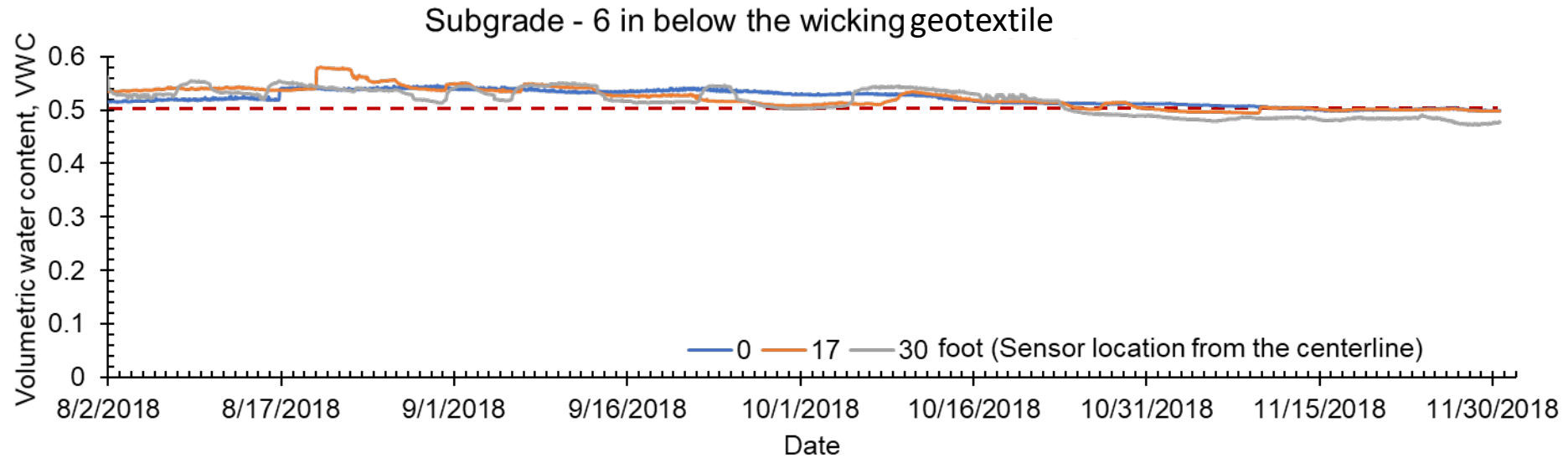
Test Section III AB3 aggregate/wicking geotextile



Frozen depth = 0.6 m (24 in)

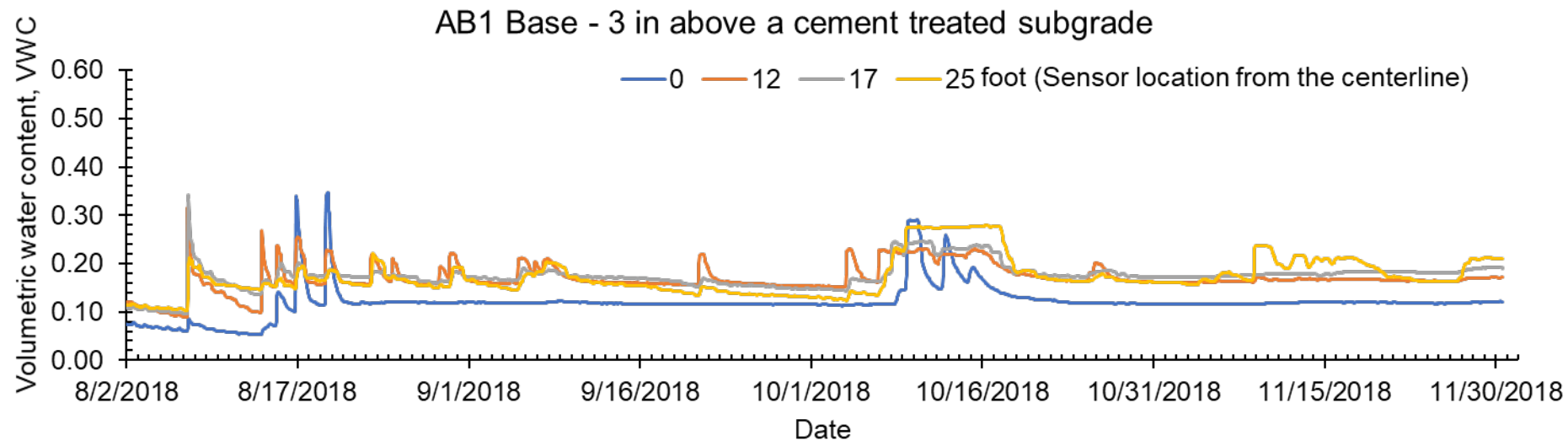
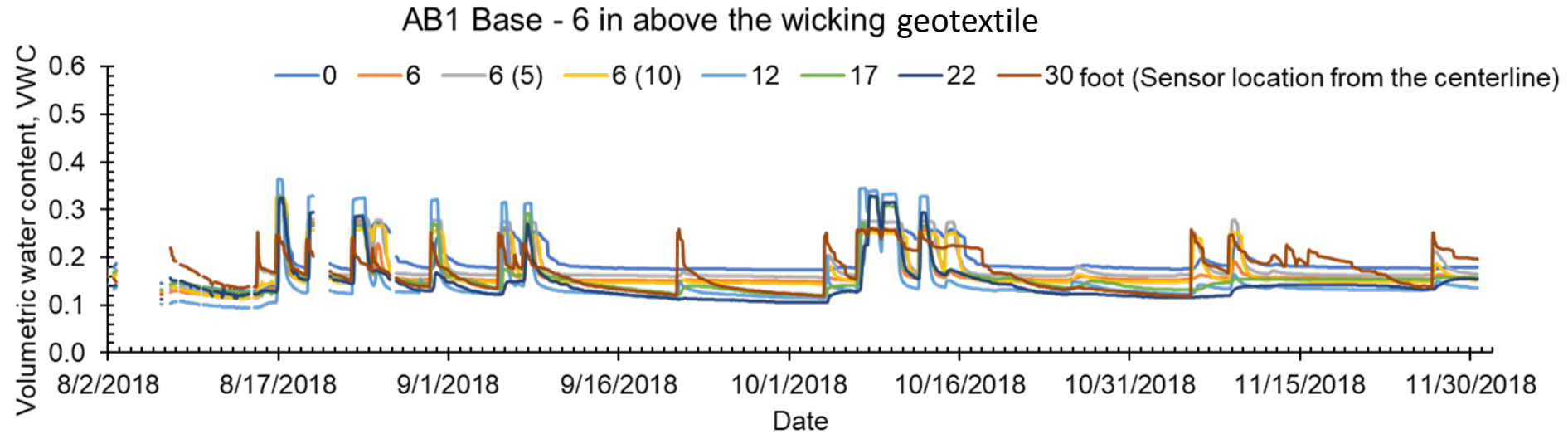
Field Monitoring Results

Test Section III: AB3 aggregate/wicking geotextile

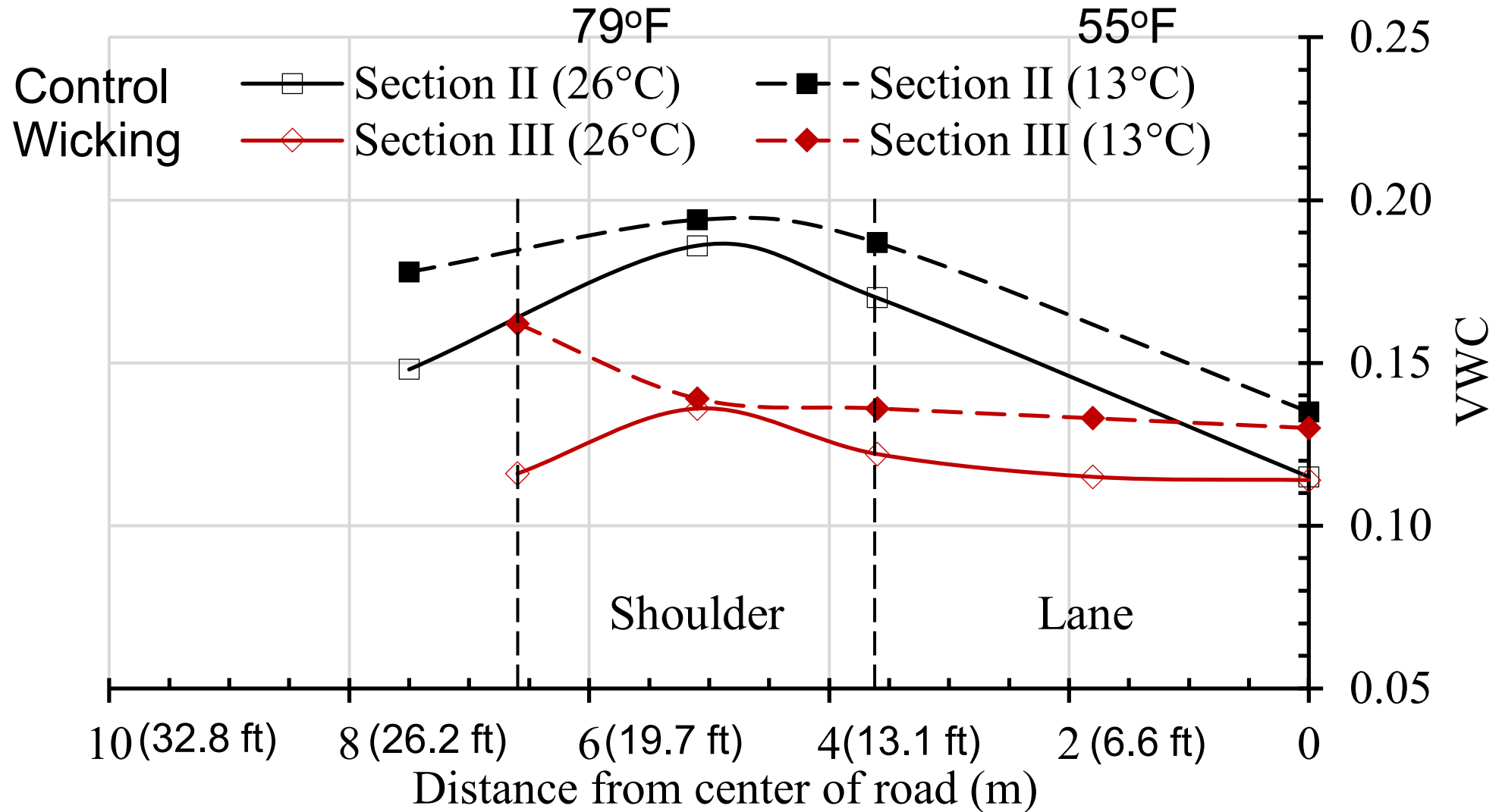


Field Monitoring Results

Test Sections I & II: AB1 aggregate/wicking geotextile & Control



Field Monitoring Results



Both evaporation and drainage reduce moisture content.

Field Monitoring Results



Section 1: wicking geotextile



Section 2: no wicking geotextile



Section 3: wicking geotextile

Concluding Remarks

- Wicking geotextile could remove water from soil under a field capacity (unsaturated).
- Wicking geotextile was more effective in reducing water content with time than non-wicking geotextile.
- The ability of wicking water from soil by the wicking geotextile depended on temperature, relative humidity, fines content, and distance to the wicking geotextile.
- The wicking geotextile significantly reduced permanent deformations of test sections under cyclic loading.
- Field studies confirmed the effectiveness of wicking geotextile in removing moisture and mitigating moisture-related road problems.

Thanks!

Questions?