

## Buck O'Neil Bridge Design-Build Project

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John Szturo, PG HNTB Geotechnical Task Leader

November 9th, 2023











## Location Map



![](_page_2_Picture_1.jpeg)

![](_page_2_Picture_2.jpeg)

as

![](_page_2_Picture_3.jpeg)

![](_page_2_Picture_4.jpeg)

# **Bridge History**

The Original Bridge was:

- Designed by HNTB
- Constructed by the City of KC, MO
- Built at a cost of \$12 million
- Opened as a toll bridge
- Opened on September 9, 1956
  "The Broadway Bridge"
- Renamed 60 years later on June 24, 2016 to "The Buck O' Neil Bridge"

![](_page_3_Picture_1.jpeg)

![](_page_3_Picture_2.jpeg)

# Buck O'Neil

- First Baseman and Manager
- for the Negro League KC Monarchs
- Long time employee and scout for the KC Royals
- Honored with the "Buck O'Neil" Legacy Seat at the K
- Inducted into the MLB Hall of fame class of 2022

![](_page_3_Picture_9.jpeg)

![](_page_4_Picture_1.jpeg)

![](_page_4_Picture_2.jpeg)

## Pre-award Work - Schedule

Advertise – April 2020

Shortlist - July 2020

Massman Clarkson HNTB

Lunda Construction

American Bridge Parsons

Traylor Ames

Walsh

Proposals Due - December 2020 Project Award - February 2021

![](_page_5_Picture_1.jpeg)

## MoDOT Design-Build Goals

- Construct an innovative, low maintenance Missouri River Bridge that will provide a century of service within a program budget of \$247.5 million.
  - Split between MoDOT and KCMO
- Provide a safe, connective and accessible transportation facility that improves regional and local system performance.
- Manage the impact to the traveling public during construction.
- Complete the project by December 1, 2024, utilizing a diverse workforce.

![](_page_6_Picture_1.jpeg)

![](_page_6_Picture_2.jpeg)

# Site Challenges

![](_page_6_Picture_4.jpeg)

![](_page_7_Picture_1.jpeg)

![](_page_7_Picture_2.jpeg)

## 8<sup>th</sup> Street Tunnel

![](_page_7_Picture_4.jpeg)

![](_page_8_Picture_1.jpeg)

![](_page_8_Picture_2.jpeg)

## 8<sup>th</sup> Street Tunnel

![](_page_8_Picture_4.jpeg)

![](_page_9_Picture_1.jpeg)

![](_page_9_Picture_2.jpeg)

## 8<sup>th</sup> Street Tunnel – Homebound

![](_page_9_Figure_4.jpeg)

![](_page_10_Picture_1.jpeg)

### Proposed Alternative – Wheeler Airport

![](_page_10_Picture_3.jpeg)

![](_page_11_Picture_1.jpeg)

![](_page_11_Picture_2.jpeg)

### Preferred Alternative – EA

![](_page_11_Figure_4.jpeg)

- 24-ft Wall20 ft from RR!!
  - Schedule/cost risk
- Righthand Exit
- Shared Use Path (SUP)

![](_page_12_Picture_1.jpeg)

### Modified Alternative – Proposed & Accepted

![](_page_12_Figure_3.jpeg)

- 24-ft Wall **70 ft** from RR
- Lefthand Exit
- Shared Use Path re-routed away from pinch-point

![](_page_13_Picture_1.jpeg)

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# AAS – Additional Appicable Standards and Design Exceptions

# Pre-Award Mark Up of MoDOT Drilled Shaft Specification

camera and lighting equipment shall be capable of operating in dry or submerged conditions encountered during the inspection. The excavated shaft shall have the engineer <u>of record</u>'s approval prior to proceeding with construction.

701.4.10.3.1 Equipment. Mathods and equipment for controlling the Inspection equipment-camera will be subject to approval from the engineer of record, and achievement of a splitfactory, video record.

701.4.10.3.2 Drawings. The contractor shall submit layout drawings to the engineer showing the relative position of all components of the video inspection system, including type and size of barge or other work area. The information submitted shall include a written description of the operating procedure in a step-by-step sequence and shall state the source of power.

701.4.10.3.3 Shaft Inspection. Inspection of a shaft by video camera shall be performed as directed by the engineer of record. The excavated shaft, including the rock socket when applicable, shall be thoroughly cleaned of all loose fragments, and sediment and turbidity prior to inspection. The camera, if used shall be operated such that optimum clarity of detail can be obtained and all surface areas of the shaft, including the rock socket and the rock socket's base, can be observed. All scanning of the rock surfaces shall be recorded. After completion of the inspection of a rock socket, the engineer of record will direct whether, or not drilling of the shaft shall be continued to a greater depth. <u>Camera Recordings, SID recordings, and all inspection records</u> shall be furnished to and shall become the property of <u>MODOT the angineer</u> upon completion of the work.

701.4.11 Foundation Inspection. NX size cores will be taken by the design build contractor and engineer of record to facilitate the characterization of the subsurface, set casing requirements and determine end bearing and side friction engineering parameters. The design build contractor's engineer of record will also confirm the design assumptions during construction and inspection of the drilled shafts. At least one NX core will be taken at each planned drilled shaft location. be required for drilled shafts with rock sockets, where NX refers to the nominal diameter of rock core, and the NX core barrel has a 2.1/8-inch inside diameter. At least 15 days prior to drilled shaft construction the contractor shall drill drill one NX size core at the center of each rock socket to a depth of 10 fest or twice the diameter of the rock socket, whichever is greater, below the bottom of the rock socket. The contractor shall use the foundation inspections holes to determine the amount of casing needed and casing ordered prior to foundation inspections holes is at the contractor's risk. The contractor may be directed to extend the rock socket to a lower elevation, resulting from the engineer <u>of record</u>'s evaluation of the foundation inspection <u>and</u> cores.

701.41.1 Log of Excavated Material. The contractor and engineer of record shall maintain a boring log of excavated material for each foundation design inspection hole. The boring logs will be included in the Project Geotechnical Report and drawings in accordance with the contract documents, and a rough draft of the logs shall be delivered to the engineer within 24 hours of completion of the boring. A typed log prepared by a geologist or engineer along with recommendations for the tip of casing shall be delivered to the engineer within Sdays. The log shall include the following:

(a) The amount of NX cored per run and the amount recovered. All core loss shall be noted and explained. Clay layers shall be noted and located on the log by depth.

(b) The Rock Quality Designation (RQD) for the NX core. The bedding thickness and degree of weathering shall also be noted.

(c) One unconfined compression test shall be run per 5 feet of NX core or as directed by the engineer of record. The results of these tests shall be delivered to the engineer. The results of the unconfined compression tests shall be reported in units of kips per square foot (ktg). Any effect on time of performance resulting from delays in delivery of the above test results to the engineer will be nonsycusable.

(d) Color photographs of the core.

701.4.11.2 Storage and Labeling of Rock Cores. Rock cores shall be stored in structurally sound core boxes and shall be protected from the elements. The core boxes shall be properly labeled to indicate location, depth, beginning elevation, contractor and date, and shall be delivered to the langineed.

701.4.12 Reinforcing Steel Cage Fabrication and Placement. The reinforcing steel cage, consisting of the longitudinal bars, ties, spirals, cage stiffener bars, spacers, centering devices, and other necessary appurtenances, shall be completely assembled as a unit, and shall be placed immediately after the shaft excavation is inspected

![](_page_14_Picture_1.jpeg)

![](_page_14_Picture_2.jpeg)

### **Pre-Award Boring Location Plan**

![](_page_14_Figure_4.jpeg)

![](_page_15_Picture_1.jpeg)

![](_page_15_Picture_2.jpeg)

## **Project Definition**

## BUCK O'NEIL BRIDGE

![](_page_15_Picture_5.jpeg)

![](_page_16_Picture_1.jpeg)

![](_page_16_Picture_2.jpeg)

### Post Award

### Design-Build Project Awarded:

### • to Massman – Clarkson – HNTB Team

• February 2021

![](_page_17_Picture_1.jpeg)

![](_page_17_Picture_2.jpeg)

### **Boring Location Plan**

![](_page_17_Picture_4.jpeg)

![](_page_18_Picture_1.jpeg)

![](_page_18_Picture_2.jpeg)

### **Combined Boring Location Plan**

![](_page_18_Picture_4.jpeg)

![](_page_19_Picture_1.jpeg)

## Subsurface Exploration Challenges

- Tight schedule
- Barge for water borings was iced in on the river in Iowa
- Starting at the height of the Covid Epidemic difficult to maintain field crews, scheduled for 4 crews, ended up with 2
- Three week stretch of Feb March cold weather
- No access to properties critical to the schedule
- Obtaining FAA permits
- Obtaining USACE permits

![](_page_20_Picture_1.jpeg)

![](_page_20_Picture_2.jpeg)

## Borings

![](_page_20_Picture_4.jpeg)

![](_page_20_Picture_5.jpeg)

![](_page_21_Picture_1.jpeg)

![](_page_21_Picture_2.jpeg)

### Water Borings

![](_page_21_Picture_4.jpeg)

![](_page_22_Picture_1.jpeg)

![](_page_22_Picture_2.jpeg)

# **Geotechnical Elements**

- A. Retaining Walls
  - 1. MSE (9)
  - 2. CIP (1)
  - 3. Concrete Block (1)
- B. Rock Slope / Wall
  - 1. Rock Bolting
  - 2. Rock Cut
  - 3. Loess Soil Slopes
  - 4. Shotcrete
  - 5. Catchment Ditch
  - 6. Soil Nail Shale

- C. Embankments
  - 1. 30-foot max. grade raise
  - 2. Lightweight Fill (LDCC)
  - 3. Stone Columns
- D. Bridge Foundations
  - 1. Driven Piles
  - 2. Pre-bored "drill and drop" Piles
  - 3. Spread Footing changed to pre-bored piles
  - 4. Drilled Shafts 78 total
    - <u>Water:</u> 11' diam., ~80 feet to rock, 30-ftlong rock sockets
    - <u>Land:</u> 8.5' and 5.5' diam.

![](_page_23_Picture_1.jpeg)

![](_page_23_Picture_2.jpeg)

## Geology

![](_page_23_Picture_4.jpeg)

![](_page_24_Picture_1.jpeg)

![](_page_24_Picture_2.jpeg)

![](_page_24_Picture_3.jpeg)

![](_page_24_Figure_4.jpeg)

![](_page_25_Picture_1.jpeg)

![](_page_25_Picture_2.jpeg)

## **Geology Profiles**

![](_page_25_Figure_4.jpeg)

![](_page_26_Picture_1.jpeg)

![](_page_26_Picture_2.jpeg)

### Case Park Wall

![](_page_26_Picture_4.jpeg)

![](_page_27_Picture_1.jpeg)

![](_page_27_Picture_2.jpeg)

### Case Park Cut and Wall

![](_page_27_Picture_4.jpeg)

![](_page_28_Picture_1.jpeg)

![](_page_28_Picture_2.jpeg)

![](_page_28_Figure_3.jpeg)

Case Park Wall

Two-tiered wall

- Top: Limestone
- •10' bench
- Bottom: Soil Nail (into shale)

![](_page_29_Figure_1.jpeg)

![](_page_29_Picture_2.jpeg)

INTE

**Case Park Wall** 

Two-tiered wall

- Top: Limestone
- •10' bench
- Bottom: Soil Nail (into shale)

![](_page_30_Picture_1.jpeg)

![](_page_30_Picture_2.jpeg)

![](_page_30_Picture_3.jpeg)

![](_page_31_Picture_1.jpeg)

![](_page_31_Picture_2.jpeg)

![](_page_31_Picture_3.jpeg)

![](_page_32_Picture_1.jpeg)

![](_page_32_Picture_2.jpeg)

![](_page_33_Picture_1.jpeg)

![](_page_33_Picture_2.jpeg)

![](_page_33_Picture_3.jpeg)

![](_page_34_Picture_1.jpeg)

![](_page_34_Picture_2.jpeg)

### South Approach Spans

![](_page_34_Figure_4.jpeg)

![](_page_35_Picture_1.jpeg)

### South Approaches - Substructure

![](_page_35_Figure_3.jpeg)

- Hammer Head Bents on
  - 8'-6" Drilled Shaft
  - 8'-0" Rock Socket
- Integral End Bents on H-Piles
  - Most Behind MSE Walls
  - One in Prebored Rock

![](_page_36_Picture_1.jpeg)

![](_page_36_Picture_2.jpeg)

### South Approach

![](_page_36_Figure_4.jpeg)

![](_page_37_Picture_1.jpeg)

![](_page_37_Picture_2.jpeg)

![](_page_37_Picture_3.jpeg)

![](_page_38_Picture_1.jpeg)

![](_page_38_Picture_2.jpeg)

![](_page_38_Picture_3.jpeg)

![](_page_39_Picture_1.jpeg)

![](_page_39_Picture_2.jpeg)

![](_page_39_Picture_3.jpeg)

![](_page_40_Picture_1.jpeg)

![](_page_40_Picture_2.jpeg)

## **River Bridges**

![](_page_40_Picture_4.jpeg)

![](_page_41_Picture_1.jpeg)

## **River Bridge - Substructure**

![](_page_41_Figure_3.jpeg)

- Design for 3,450-kip Vessel Collision Load (per RFP)
- Design for Scour to Bedrock (per RFP)
- Waterline Strut
- 5 ksi Concrete
- 11'-0" Drilled Shafts
- 10'-6" Rock Sockets
- Bedrock: PLEASANTON SHALE

![](_page_42_Picture_1.jpeg)

![](_page_42_Picture_2.jpeg)

### **Nearby Load Tests in Pleasanton**

![](_page_42_Picture_4.jpeg)

![](_page_43_Picture_1.jpeg)

![](_page_43_Figure_3.jpeg)

![](_page_43_Figure_4.jpeg)

![](_page_44_Picture_1.jpeg)

CONSTRUCTION CO. CONSTRUCTION COMPANY

HNTB

![](_page_44_Picture_3.jpeg)

For shale with UCS ~ 60 ksf, Nom. Unit Side Resist. = 7.4 ksf < 15 ksf

For shale with UCS ~ 170 ksf, Nom. Unit Side Resist. = 12.4 ksf < 16 ksf

![](_page_44_Figure_6.jpeg)

![](_page_45_Picture_1.jpeg)

![](_page_45_Figure_3.jpeg)

![](_page_46_Picture_1.jpeg)

![](_page_46_Figure_2.jpeg)

![](_page_47_Picture_1.jpeg)

### River Bridge - Northbound Main Span

![](_page_47_Figure_3.jpeg)

![](_page_48_Picture_1.jpeg)

![](_page_48_Picture_2.jpeg)

### North Approach Spans

![](_page_48_Picture_4.jpeg)

![](_page_49_Picture_1.jpeg)

## SB North Approach by Airport

![](_page_49_Figure_3.jpeg)

### Wrap Around MSE Walls

- 27' Tall at Abutment
- 8' to 15' of Clay & Sand FILL with gravel, cinders & brick; over Soft Fat Clay to 18'

### **Stone Columns to Mitigate**

- Short-term Bearing,
- Short-term Global, and
- Variable, Slow Settlement

![](_page_50_Picture_1.jpeg)

# MSE Wall at 3<sup>rd</sup> St. (South Approach)

![](_page_50_Figure_3.jpeg)

![](_page_51_Picture_1.jpeg)

# MSE Wall at 3<sup>rd</sup> St.

![](_page_51_Figure_3.jpeg)

 In the RED ZONE, overexcavation limited to 4 ft below existing ground (i.e. 2 ft below B/Wall).

MASSMAN CLARKSON CONSTRUCTION CO. CONSTRUCTION COMPANY

- Lean Clay Embankment
  - SB first then NB.
- TRY: Low Density Cellular Concrete (LDCC) where needed (RED ZONE).
  - Cast unit weight = 30 pcf
  - Phi design = 35 deg.

![](_page_52_Picture_1.jpeg)

![](_page_52_Picture_2.jpeg)

# MSE Wall at 3<sup>rd</sup> St.

Photos of previous use of LDCC at nearby US-24 over Delaware Street

![](_page_52_Picture_5.jpeg)

![](_page_52_Picture_6.jpeg)

![](_page_53_Picture_1.jpeg)

HNTB

A JOINT VENTURE

## MSE Wall at 3<sup>rd</sup> St. - Stability

![](_page_53_Figure_3.jpeg)

![](_page_54_Picture_1.jpeg)

# MSE Wall at 3<sup>rd</sup> St. - Stability

### LDCC in Light Blue Zone:

- for Short-term Bearing
- to Limit Risk of Excess Settlement of Wall and Utilities.

LDCC in Med. Blue Zone (behind the 1:1 wedge):

 for Short-term & Long-term Global

![](_page_54_Figure_8.jpeg)

### 2' Gravel in Orange Zone:

for Drainage & Sliding Stability

![](_page_55_Picture_1.jpeg)

## MSE Wall at 3<sup>rd</sup> St. – Settlement

Figure B: Isometric View of South Approach Embankment Loads as Modeled in Settle3

![](_page_55_Figure_4.jpeg)

Along face of wall: Predicted Settlement = 2 to 3 inches.

Along 48" Sewer: Predicted Settlement < 1.5 inches.

At the shorter SB approach (20 ft fill): Predicted Settlement = 10 inches. Measured Settlement = 2 inches!

![](_page_56_Picture_1.jpeg)

![](_page_56_Picture_2.jpeg)

# Construction Photos

![](_page_56_Picture_4.jpeg)

![](_page_57_Picture_1.jpeg)

![](_page_57_Picture_2.jpeg)

![](_page_57_Picture_3.jpeg)

![](_page_58_Picture_1.jpeg)

![](_page_58_Picture_2.jpeg)

![](_page_58_Picture_3.jpeg)

![](_page_59_Picture_1.jpeg)

![](_page_59_Picture_2.jpeg)

![](_page_59_Picture_3.jpeg)

![](_page_60_Picture_1.jpeg)

![](_page_60_Picture_2.jpeg)

![](_page_60_Picture_3.jpeg)

![](_page_61_Picture_1.jpeg)

![](_page_61_Picture_2.jpeg)

![](_page_61_Picture_3.jpeg)

![](_page_62_Picture_1.jpeg)

![](_page_62_Picture_2.jpeg)

![](_page_63_Picture_1.jpeg)

![](_page_63_Picture_2.jpeg)

![](_page_63_Picture_3.jpeg)

![](_page_64_Picture_1.jpeg)

![](_page_64_Picture_2.jpeg)

### Questions

![](_page_64_Picture_4.jpeg)